

## Transport in a coordinated soil-root-xylem-phloem leaf system

Cheng-Wei Huang<sup>a,\*</sup>, Jean-Christophe Domec<sup>b,c</sup>, Sari Palmroth<sup>b</sup>, William T. Pockman<sup>a</sup>,  
Marcy E. Litvak<sup>a</sup>, Gabriel G. Katul<sup>b,d,e</sup>

<sup>a</sup> Biology Department, University of New Mexico, Albuquerque, NM, USA

<sup>b</sup> Nicholas School of the Environment, Duke University, Durham, NC, USA

<sup>c</sup> UMR INRA-ISP 1391, Bordeaux Sciences Agro, Gradignan 33195, France

<sup>d</sup> Department of Civil and Environmental Engineering, Duke University, Durham, NC, USA

<sup>e</sup> Karlsruhe Institute of Technology (KIT), Institute of Meteorology and Climate Research, Kreuzeckbahnstr. 19, Garmisch-Partenkirchen 82467, Germany

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### ABSTRACT

Links between the carbon and water economies of plants are coupled by combining the biochemical demand for atmospheric CO<sub>2</sub> with gas transfer through stomates, liquid water transport in the soil-xylem hydraulic system and sucrose export in the phloem. We formulated a model to predict stomatal conductance ( $g_s$ ), consistent with the maximum energy circulation concept of Lotka and Odum, by maximizing the sucrose flux out of photosynthesizing leaves. The proposed modeling approach recovers all prior results derived from stomatal optimization theories and profit-maximization arguments for the xylem hydraulic system aimed at predicting  $g_s$ . The novel features of this approach are its ability to 1) predict the price of losing water in carbon units using xylem and phloem properties (i.e., the marginal water use efficiency) and 2) explain why water molecules become more expensive to exchange for CO<sub>2</sub> molecules when soil moisture becomes limiting or when plants acclimate to new elevated atmospheric CO<sub>2</sub> concentration. On short time-scales (sub-daily), predicted  $g_s$  under many environmental stimuli were consistent with measurements reported in the literature, including a general sensitivity of  $g_s$  to vapor pressure deficit and leaf water potential. During progressive droughts, differences in the coordination among the leaf, xylem, and phloem functioning determine the isohydric-to-anisohydric behavior among plants.

### 1. Introduction

Stomata evolved more than 400 million years to regulate gas exchange with a desiccating atmosphere, allowing land plants to spread across the earth's surface. Environmental responses of stomata are now prominently featured as a research priority in many studies on climate change, food security, and food-energy-water nexus (Betts et al., 2007; Cox et al., 2000; Gedney et al., 2006; Hetherington and Woodward, 2003). As plants adapted to a terrestrial environment, they competed for light and utilized increasing height to enhance their capacity to photosynthesize. Height facilitates a productive display of photosynthetic machinery by allowing a vertical distribution of chlorophyll so that light-use efficiency can be increased relative to a concentrated display of chlorophyll (Gratani, 2014). Increased height further required selection for solutions to improve water delivery to leaves and carbohydrate translocation from leaves to reserves, root exudation, and export to symbionts (Fatichi et al., 2014; Pittermann, 2010; Thompson and Katul, 2012).

It is now accepted that a framework linking stomatal function to such water delivery and translocation of carbohydrates is needed to assess

how vegetation structure and its spatial patterns is impacted by future climate conditions, and vice versa (Hölttä et al., 2017; Jensen et al., 2016; Mencuccini and Hölttä, 2010; Nikinmaa et al., 2013; Savage et al., 2015; Sevanto, 2014; Sperry and Love, 2015). The general features of this framework rely upon the cohesion-tension (CT) theory of sap ascent in the xylem (Dixon and Joly, 1895), osmosis and pressure-driven transport in the phloem through the Münch mechanism (Jensen et al., 2016), and stomatal optimization theories (SOT) in leaves linking the carbon and water economies of plants (Cowan and Farquhar, 1977). The latter approach, while lacking the physical basis of the other two, has been reasonably successful in explaining short-term responses of leaf gas-exchange to variations in photosynthetically active radiation (PPFD), air temperature ( $T_a$ ), atmospheric CO<sub>2</sub> concentration ( $c_a$ ), and atmospheric aridity (Buckley et al., 2016; Damour et al., 2010; Katul et al., 2012; 2009; Medlyn et al., 2011; Paschalis et al., 2017). Because stomatal function balances photosynthetic carbon gain and water loss (transpiration) to the atmosphere, a number of arguments have been offered to displace the original SOT at the leaf scale (Cowan and Farquhar, 1977). At the whole-plant level, soil-xylem hydraulics (i.e., outcome of supply and demand for water) and carbohydrate (mainly

\* Corresponding author.

E-mail addresses: [ch224@unm.edu](mailto:ch224@unm.edu) (C.-W. Huang), [jc.domec@duke.edu](mailto:jc.domec@duke.edu) (J.-C. Domec), [sari.palmroth@duke.edu](mailto:sari.palmroth@duke.edu) (S. Palmroth), [pockman@unm.edu](mailto:pockman@unm.edu) (W.T. Pockman), [mlitvak@unm.edu](mailto:mlitvak@unm.edu) (M.E. Litvak), [gaby@duke.edu](mailto:gaby@duke.edu) (G.G. Katul).

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sucrose) transport efficiency in the phloem impose appreciable constraints so as to govern leaf-level gas exchange (Hölttä et al., 2017; 2006; Jensen et al., 2016; Mencuccini and Hölttä, 2010; Nikinmaa et al., 2013; Savage et al., 2015; Sevanto, 2014; Sperry and Love, 2015).

The work here shows that the original SOT at the leaf scale (Cowan and Farquhar, 1977), the maximization of water flow in the xylem (and variants on them), the maximization of carbohydrate transport, and attainment of a near-constant inter-cellular to ambient atmospheric CO<sub>2</sub> hypothesis (Prentice et al., 2014) all lead to similar formulations for stomatal conductance under well-watered soil condition. What is different across these approaches is the interpretation of parameters (e.g., the cost term used to maximize or minimize the objective function) and their short-term responses to boundary conditions such as root-zone soil moisture and changes in  $c_a$ . Despite differences in what these approaches maximize (or minimize), a similarity in outcome may be hinting that a more general principle is governing plant responses to fluctuating environmental conditions, the main focus of the work here.

Our conjecture is that plants may have evolved a coordinated photosynthetic-hydraulic-sucrose transporting machinery that confers some competitive advantages in fluctuating environmental conditions. Such a coordination should manifest itself in linkages between the properties describing the photosynthetic machinery, the hydraulic and carbohydrate transporting systems. It will be remiss if analogies to the energetics of evolution principle as a consequence of natural selection, proposed in 1922 by Lotka (Lotka, 1922; Odum and Hall, 1995), are not pointed out. This principle states that “Natural selection tends to make the energy flux through the system a maximum, so far as compatible with the constraints to which the system is subject.” As indicated by Lotka, the maximum input of energy flux exceeding the actual energy demand (for growth, maintenance, defense and reproduction) at the current states offers a great opportunity in the future to develop an advantageous plant body that can promote larger total energy flux through the system. In the plant kingdom, the input of energy flux can be expressed as the sucrose flux rendered out of the loading leaf. Environmental conditions and endogenous transport processes affecting this energy flux represent the limiting constraints to the system. It is with this view that coordination among the xylem, phloem, and leaf is interpreted as an energy-capturing device to direct available energy into the system by harvesting limited resources (Lotka, 1922).

### 1.1. Hypothesis

In light of the energetics of the evolution principle (Lotka, 1922), we hypothesize that stomatal conductance ( $g_s$ ) can be predicted by assuming coordination in the leaf-xylem-phloem system thereby recovering the mathematical form of the aforementioned approaches. The criterion for predicting  $g_s$  is that this coordination maintains efficient (maximum) transport rate of photoassimilates (i.e., energy flux) out of the loading zone over short time intervals ( $\Delta t$ ) so as to ensure maximum energy circulation at the whole-plant level. When coupling the transport and physiological processes in the leaf-xylem-phloem system (i.e., photosynthetic machinery, water transport in xylem and export of assimilated sugar from loading phloem), how the limiting constraints induced by these processes and their interaction impact the energy flux entering the plant system and subsequently  $g_s$  are now considered explicitly in this new modeling approach. Specifically, this hypothesis offers a number of advantages: (1) the phloem transport efficiency is no longer isolated from the photosynthetic machinery, soil-xylem hydraulics and stomatal function as is now recognized (Hölttä et al., 2017; Jensen et al., 2016; Mencuccini and Hölttä, 2010; Nikinmaa et al., 2013; Sevanto et al., 2014); (2) the hypothetical assumption of pricing water loss in SOT or fitness costs of low xylem water potential in profit-maximization is by-

passed. It should be noted that the transport rate of photoassimilates out of the loading zone represents the objective function to be maximized, which is similar to the non-steady state model proposed elsewhere (Nikinmaa et al., 2013). Adopting this hypothesis, the objective of this work is to analyze  $g_s$  responses to environmental factors and plant attributes across a wide range of time-scales. We also focus specifically on two consequences of the model results: (i) The  $g_s$  responses to long-term elevated-CO<sub>2</sub> conditions and (ii) progressive drought as well as species differentiation across the spectrum of isohydric-to-anisohydric behavior. Before presenting the model formulation, the constraints on photosynthesis and xylem-water movement are briefly reviewed with a lens on their connections.

### 1.2. Constraints on photosynthesis and water transport

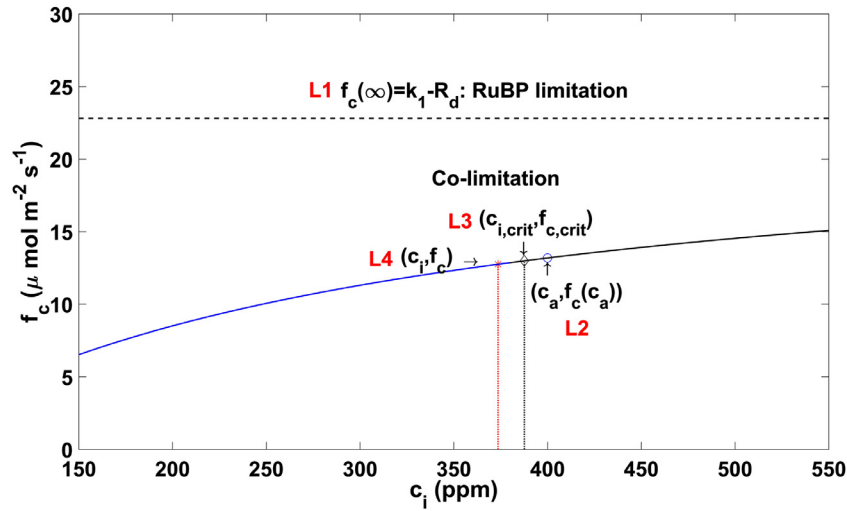
For C3 plants, the photosynthetic machinery limits the biochemical demand for CO<sub>2</sub> ( $f_{c,d}$ ). Mathematically,  $f_{c,d}$  can be expressed as the outcome of co-limitation of Ribulose-1,5-bisphosphate carboxylase/oxygenase (Rubisco) kinetic activity and Ribulose-1,5-bisphosphate (RuBP) regeneration rate (Farquhar et al., 1980b) approximated by Vico et al. (2013):

$$f_{c,d} = \frac{k_1(c_i - \Gamma^*)}{k_2 + c_i} - R_d, \quad (1)$$

where  $c_i$  is the inter-cellular CO<sub>2</sub> concentration,  $k_1$  and  $k_2$  are photosynthetic parameters that vary with PPFD and  $T_a$ ,  $\Gamma^*$  is the CO<sub>2</sub> compensation point in the absence of mitochondrial respiration, and  $R_d$  is the daytime mitochondrial respiration rate. Eq. (1) is a hyperbolic function imposing the most limiting factor through electron transport rate at high  $c_i$  (i.e.,  $f_{c,d} \approx J/4 - R_d$  when  $k_1 = J/4$  where  $J$  is the electron transport rate) or through Rubisco activity at low  $c_i$  (i.e.,  $f_{c,d} \approx V_{c,max}(c_i - \Gamma^*)/(c_i + a_2) - R_d$  when  $k_2 = k_1 a_2 / V_{c,max}$  where  $V_{c,max}$  is the maximum carboxylation capacity and  $a_2 = K_c(1 + C_{oa}/K_o)$  where  $C_{oa}$  is the oxygen concentration in the atmosphere and  $K_c$  and  $K_o$  are respectively the Michaelis constants for CO<sub>2</sub> fixation and oxygen inhibition (Vico et al., 2013). When operating under co-limitation regime, Eq. (1) also ensures a continuous transition between the two photosynthetic limitations. For  $c_i \rightarrow \infty$ ,  $f_{c,d}$  saturates at a maximum  $f_{c,max} = k_1 - R_d$  (i.e., the asymptotic behavior of  $f_c - c_i$  curve;  $f_{c,d}|_{c_i \rightarrow \infty} = k_1(c_i - \Gamma^*)/(k_2 + c_i) - R_d|_{c_i \rightarrow \infty}$ ). Hence, when  $c_i$  availability is not limiting, photosynthesis is only constrained by the photosynthetic machinery usually through electron transport (RuBP limitation; L1 in Fig. 1). Although an infinite  $c_i$  is not realistic for any condition, this extreme case may be used to explain the rapid land colonization by plants in the Ordovician and their subsequent productivity during the Silurian-Devonian approximately 400 million years ago. During this time period,  $c_a$  reached up to 5000 ppm (Berner, 1991; Berner and Kothavala, 2001) and the long-term  $c_i/c_a$  commonly ranged from 0.6 to 0.9 (Drake et al., 1997; Ehleringer and Cerling, 1995; Prentice et al., 2014; Wong et al., 1979). It was this era when photorespiration was potentially suppressed and water use efficiency remained high (Sperry, 2003).

For present  $c_a$  conditions ( $\approx 400$  ppm), the assimilation rate is further limited by the atmospheric supply of CO<sub>2</sub>, which in turn is governed by  $c_a$ , the transport efficiency to CO<sub>2</sub> through the stomatal pathway (i.e., stomatal conductance;  $g_s$ ), and the laminar boundary layer attached to the leaf surface. Assuming an infinitesimal thickness of the laminar boundary layer (i.e., well-coupled condition) and a mesophyll conductance to CO<sub>2</sub> that is much larger than  $g_s$ , the atmospheric supply of CO<sub>2</sub> across the stomatal aperture can be described by a Fickian diffusion and is given as  $f_{c,s} = g_s(c_a - c_i)$ . If all CO<sub>2</sub> molecules diffusing through stomata are eventually assimilated, then the supply and demand for CO<sub>2</sub> are in balance resulting in  $f_{c,s} = f_{c,d}$ . The  $f_{c,s} = f_{c,d}$  results in an actual photosynthetic rate ( $f_c$ ) that can then be expressed as a function of  $g_s$  and the photosynthetic parameters (Huang et al., 2015; Katul et al., 2010):

$$f_c(g_s) = \frac{1}{2}[k_1 + (k_2 + c_a)g_s - R_d]$$



**Fig. 1.** The biochemical demand ( $f_c - c_i$ ) curve featuring the various mechanisms (L1–L4) limiting photosynthesis (L1: limitation of the photosynthetic machinery when  $c_i \rightarrow \infty$ , L2: limitation of atmospheric  $\text{CO}_2$  concentration when  $c_i \rightarrow c_a$ , L3: soil–xylem hydraulic limitation representing the maximum permissible  $f_{c, \text{crit}}(c_{i, \text{crit}})$  at critical  $\psi_{i, \text{crit}}$ , L4: limitation of a coordinated photosynthetic–hydraulic–sucrose transporting machinery). How these limitations (i.e., L1–L4) impact  $f_c$  that can operate along the  $f_c - c_i$  curve is presented. The physiological, hydraulic and allometric attributes of soil–plant system for coniferous species in general reported elsewhere (Huang et al., 2017) are adopted. The  $K - \psi_i$  is reconstructed using a multi-layer plant hydraulic model described elsewhere (Huang et al., 2017; Sperry et al., 1998). Physical characteristics of leaves and anatomical attributes of phloem for *Pinus taeda* L. listed in Table 2 are used. The sugar loading efficiency ( $\alpha$ ) is assumed to be 1 (Hölttä et al., 2017; Nikinmaa et al., 2013). The result here is computed for well-watered soil condition when photosynthetically active radiation (PPFD), air temperature ( $T_a$ ), atmospheric  $\text{CO}_2$  concentration ( $c_a$ ) and relative humidity ( $RH$ ) are  $1000 \mu\text{mol m}^{-2} \text{s}^{-1}$ ,  $25^\circ\text{C}$ ,  $400 \text{ ppm}$  and  $90\%$ , respectively.

$$-\sqrt{[k_1 + (k_2 - c_a)g_s - R_d]^2 - 4g_s(-c_a g_s k_2 - k_2 R_d - k_1 \Gamma^*)}]. \quad (2)$$

For  $g_s \rightarrow \infty$  (i.e., stomata do not limit photosynthesis),  $c_i \rightarrow c_a$  and a finite maximum  $f_c = k_1(c_a - \Gamma^*)/(k_2 + c_a) - R_d$  is guaranteed (see Eq. (1)). Again, this is another reference condition where  $f_c$  is now bounded by finite  $c_a$  (L2 in Fig. 1). When  $c_a \rightarrow \infty$ ,  $f_{c, \text{max}}$  is recovered. For a finite  $g_s$ ,  $f_c$  is limited by  $g_s$  (see Eq. (2)) as well as environmental conditions through their effects on  $k_1$ ,  $k_2$ , and  $\Gamma^*$ . As shown later, such limitations are dictated by the coordinated photosynthetic–hydraulic–sucrose transporting machinery. Eq. (2) demonstrates that an additional and independent link between  $f_c$  and  $g_s$  is needed to mathematically solve for  $g_s$ ,  $f_c$ , and  $c_i$  from  $(c_i/c_a) = 1 - f_{c,s}/(g_s c_a)$ . In current climate and land-surface models, this independent expression is provided using one of two semi-empirical formulations proposed by Ball et al. (1987) (BWB) and Leuning (1995) (LEU) thereby allowing  $f_c$ ,  $g_s$ , and  $c_i$  to be predicted (Baldocchi and Meyers, 1998; Juang et al., 2008; Lai et al., 2000; Sellers et al., 1996; 1995; Siqueira and Katul, 2002). The common feature of BWB and LEU models is that  $g_s = m_E(f_c/(c_a - \Gamma^*))F$  where  $m_E$  is an empirical parameter linking  $g_s$  to  $f_c/(c_a - \Gamma^*)$  and the reduction function  $F = RH$  or  $(1 + D/D_0)^{-1}$  is an atmospheric aridity function where  $RH$  is the relative humidity,  $D$  is the vapor pressure deficit, and  $D_0$  is a normalizing constant. How  $g_s$  is impacted by the measures of atmospheric aridity such as  $RH$  and  $D$  is included in BWB and LEU models. The linkage between  $g_s$  and  $f_c/c_a$  through  $F$  is perhaps not surprising when water loss through the stomatal pathway (i.e., atmospheric evaporative demand;  $f_{e,d} \approx a g_s D/P_a$  where  $a \approx 1.6$  is the relative diffusivity of water vapor with respect to  $\text{CO}_2$  and  $P_a$  is the atmospheric pressure.) is inevitable during photosynthesis. The  $g_s$  should satisfy both the atmospheric evaporative demand (i.e.,  $f_{e,d}$ ) and the supply–demand balance of  $\text{CO}_2$  (i.e.,  $f_{c,s} = f_{c,d}$ ; Eq. (2)).

Such atmospheric evaporative loss from the leaf as driven by the biochemical demand for  $\text{CO}_2$  and the aridity of the atmosphere only serves as an upper bound for water vapor loss. The actual water supply to satisfy the atmospheric evaporative demand also depends on soil water availability and whole-system hydraulic conductance ( $K$ ) integrated throughout the entire water flow path commencing from the soil and progressing to the distal parts of the plants (Sperry and Love, 2015). When xylem water potential decreases, originally functional (i.e., water-

filled) xylem conduits can be occupied by air drawn from neighboring air-filled conduits through inter-conduit pit membranes such that water is no longer conducted by these dysfunctional conduits (Crombie et al., 1985; Sperry and Tyree, 1988; 1990). Similar to xylem, soil water conductivity that varies with decreasing water potential is also reduced by spreading air over pore space between soil particles. The BWB and LEU models do not explicitly or mechanistically consider how  $g_s$  is impacted by reductions in  $K$  due to progressive soil drying (i.e., soil–xylem hydraulic limitation). The effects of such soil drying is represented by ad-hoc reductions in  $m_E$  (Tuzet et al., 2003).

Based on the economics of leaf-level gas exchange (Berninger and Hari, 1993; Cowan and Farquhar, 1977; Givnish and Vermeij, 1976; Hari et al., 1986; Konrad et al., 2008), stomatal optimization theories (SOT) provide an alternative approach to predict  $g_s$ . In SOT, the stomatal aperture variation is assumed to maximize carbon gain subjected to a ‘cost’ of water loss incurred during transpiration in carbon units (cost function). This constrained optimization theory is equivalent to maximizing the objective function (or Hamiltonian) defined as:

$$H_{a,L}(g_s) = \underbrace{f_c(g_s)}_{\text{Gain}} - \underbrace{\lambda_L f_{e,d}(g_s)}_{\text{Cost}}, \quad (3)$$

$$\frac{\partial H_{a,L}(g_s)}{\partial g_s} = \frac{\partial f_c(g_s)}{\partial g_s} - \lambda_L \frac{\partial f_{e,d}(g_s)}{\partial g_s} = 0,$$

with  $(\partial f_c/\partial g_s)/(\partial f_{e,d}/\partial g_s) = \lambda_L > 0$ , where the cost function is determined by the unit cost of water loss,  $\lambda_L$ , also known as the marginal water use efficiency (or Lagrange multiplier). Under some conditions, the analytical form of  $g_s$  derived from SOT is *per se* similar to BWB and LEU models (Katul et al., 2010; 2012; Medlyn et al., 2011; Volpe et al., 2011). For the optimal solution to hold,  $\lambda_L$  must be a constant independent of short-term stomatal aperture fluctuations (e.g., sub-hourly) (Katul et al., 2009). However,  $\lambda_L$  may vary on longer time-scales such as those commensurate with drying soil (daily), or any structural acclimation or adaptation (monthly or yearly) (Buckley et al., 2016; Manzoni et al., 2013b). Stated differently,  $\lambda_L$  can be inferred from  $(\partial f_c/\partial g_s)/(\partial f_{e,d}/\partial g_s)$  provided a large time-scale separation exists between the  $g_s$ - and  $\lambda_L$ -variability (Katul et al., 2010; Manzoni et al., 2011). Similar to BWB and LEU models, the representation of water loss in SOT ( $f_{e,d}$ ) does not

directly account for water supply limitations imposed by the soil-xylem hydraulic system (Wolf et al., 2016). To capture such effects in drying soil conditions, an ad-hoc increase in  $\lambda_L$  with decreasing soil water status must be *a priori* specified (Manzoni et al., 2011). Soil-xylem hydraulics may offer a logical alternative to such ad-hoc specification.

A linkage between  $g_s$  and soil-xylem hydraulics can be obtained by the supply-demand balance for water (Manzoni et al., 2014; Sperry and Love, 2015; Sperry et al., 2016b) given as:

$$f_{e,s} = \frac{K(\psi_l)[\psi_s - \psi_l]}{m_v A_l} = \frac{a g_s D}{P_a} = f_{e,d}, \quad (4)$$

$$\text{resulting in } g_s(\psi_l) = \frac{K(\psi_l)[\psi_s - \psi_l] P_a}{a D m_v A_l},$$

where  $f_{e,s}$  represents the steady-state water supply function determined by the overall  $K(\psi_l)$  and the total water potential difference between the soil ( $\psi_s$ ) and the leaf xylem ( $\psi_l$ ),  $m_v$  is the molecular weight of water, and  $A_l$  is the leaf area. When coupling the supply-demand balance of  $\text{CO}_2$  (Eq. (2)) and water (Eq. (4)) fluxes through  $g_s$ , an  $f_c(\psi_l)$  relation can be derived without invoking a cost function and its associated unknown parameter,  $\lambda_L$ , as in SOT. However,  $\psi_l$  is now necessary to determine  $f_c$  prompting interest in possible links between SOT and soil-xylem hydraulics.

As a necessary step to link soil-xylem hydraulics to SOT, two remarks are in order: (1)  $g_s$  is entirely described by  $\psi_l$  at a given  $\psi_s$  as given by Eq. (4) provided that the  $K(\psi_l)$  is known, and (2)  $f_c(g_s)$  is a monotonically increasing function with increasing  $g_s$  as dictated by Eq. (2). These two remarks imply that  $f_c(g_s)$  is a maximum at the maximum  $g_s$  allowed by Eq. (4) and this maximum can be evaluated from  $\partial g_s / \partial \psi_l = 0$ . The associated leaf pressure satisfying  $\partial g_s / \partial \psi_l = 0$  is hereafter referred to as  $\psi_{l, \text{crit}}$ . The water and  $\text{CO}_2$  fluxes at  $\psi_{l, \text{crit}}$  must represent the maximum permissible water transport capacity ( $f_{e, \text{crit}}$ ) and the maximum permissible assimilation rate ( $f_{c, \text{crit}}$ ) that can be supported by the soil-xylem hydraulic system to the leaf at a given  $\psi_s$  (Manzoni et al., 2013a; Sperry et al., 2002). To solve the equation  $\partial g_s / \partial \psi_l = 0$  and determine  $\psi_{l, \text{crit}}$ ,  $K(\psi_l)$  must be *a priori* determined. There are multiple approaches to determine  $K(\psi_l)$  at the plant scale that often necessitate detailed hydraulic models through the soil-root-xylem system (Bohrer et al., 2005; Huang et al., 2017; Manoli et al., 2014; Sperry et al., 1998). Notwithstanding this complication,  $K(\psi_l)$  can be determined independently without requiring any knowledge of the photosynthetic properties or atmospheric drivers for  $g_s$ . Hence, unless otherwise stated, it is assumed that  $K(\psi_l)$  is known and represents the up-scaled xylem hydraulic system. The supply-demand balance of water flux sets another physical limit on  $g_s$  because of  $f_{e, \text{crit}}$  and thus  $f_c$  (L3 in Fig. 1). Last, it is to be noted that maximizing  $f_c(\psi_l)$  is equivalent to maximizing  $f_e(\psi_l)$ . This further suggests that the consideration of supply-demand balance of  $\text{CO}_2$  (Eq. (2)) and water (Eq. (4)) fluxes alone is not sufficient to predict the operating  $g_s$  and  $f_c$  (i.e., operating  $f_c$  is smaller than  $f_{c, \text{crit}}$ ; L4 in Fig. 1). Moreover, the operating leaf pressure must be larger than  $\psi_{l, \text{crit}}$  (or smaller in magnitude). To be shown later, the limitations in the coordinated photosynthetic-hydraulic-sucrose transporting system are required to determine the optimal operating leaf pressure for a given soil pressure.

A number of variants to this approach have also been proposed. For example, a modified SOT that accounts for the soil-xylem hydraulics can be expressed as (Novick et al., 2016):

$$\underbrace{H_{a,X}(\psi_l)}_{\text{Profit}} = \underbrace{f_c(\psi_l)}_{\text{Gain}} - \underbrace{\lambda_X f_e(\psi_l)}_{\text{Cost}} \quad (5)$$

$$\frac{\partial H_{a,X}(\psi_l)}{\partial \psi_l} = \frac{\partial f_c(\psi_l)}{\partial \psi_l} - \lambda_X \frac{\partial f_e(\psi_l)}{\partial \psi_l} = 0.$$

Because  $g_s$  is entirely described by  $\psi_l$ , Eq. (5) can be directly derived from Eq. (3) by noting that  $\partial H_{a,X} / \partial g_s = (\partial H_{a,X} / \partial \psi_l)(\partial \psi_l / \partial g_s) = 0$  is equivalent to  $(\partial H_{a,X} / \partial \psi_l) = 0$  when  $|\partial \psi_l / \partial g_s|$  is always larger than zero (see Eq. (4)). The cost function in Eq. (5) represents the sought-after limitation on  $g_s$  and further includes soil-xylem hydraulics. As the modified

SOT explicitly accounts for the soil-xylem hydraulics at the whole-plant level to accommodate the effects of dry soil process (i.e., varying  $\psi_s$  and  $\psi_l$ ) on  $g_s$ , Eq. (5) may be robust as  $\lambda_X$  is expected to be less variable when compared with its leaf-level  $\lambda_L$  counterpart in the conventional SOT. A pre-specified increasing function of  $\lambda_L$  with decreasing  $\psi_s$  is still required as discussed before. However, the specification of  $\lambda_X$  remains arbitrary. Another approach that bypasses the need for specifying  $\lambda_X$  altogether is to revise the objective function. A matrix of marginal xylem tension efficiency (Wolf et al., 2016) or relative  $K$  losses (Sperry et al., 2016a) were recently suggested as alternatives to SOT (and are labeled as profit-maximization). Their mathematical form can be still framed explicitly as *Gain-Cost* thereby resembling  $H_{a,X}$  but without the need for a  $\lambda_X$ . Next, sucrose production (by-product of photosynthesis) and their transport in the phloem may offer new constraints on the leaf-xylem hydraulic system (or the marginal water use efficiency) thereby mathematically closing the original problem linking xylem-leaf-phloem discussed in Section 1.

## 2. Theory

### 2.1. Modeling framework

The leaf-level gas exchange of water vapor and  $\text{CO}_2$ , liquid water, and carbohydrate (assumed to be sucrose) mass fluxes in xylem and phloem are presented in Fig. 2 (a). The notations and units used throughout are listed in Table 1. As noted earlier, the relation between  $K$  and  $\psi_l$  here (see Eq. (4)) is reconstructed using a multi-layer plant hydraulic model described elsewhere (Huang et al., 2017; Sperry et al., 1998) and is not repeated. The basic elements of this hydraulic model are as follows: Hydraulic architecture for both above- and below-ground compartments are not explicitly resolved but indirectly accounted for in the whole-system hydraulic conductance (i.e.,  $K(\psi_l)$ ). The effects of plant water storage and hysteresis in  $K - \psi_l$  relation induced by the delay in repair of cavitated xylem conduits (i.e., refilling) are also not considered here (see Section 3.4) but can be accommodated in the present framework. A number of features are pointed out regarding the numerical solution of the hydraulic model (i.e.,  $K - \psi_l$  relation): 1) the leaf water potential  $\psi_{12}$  at which hydraulic conductivity drops by 12% from its maximum value  $K_{\text{max}}$  can be determined from the derived  $K - \psi_l$  relation and roughly coincides with the air-entry pressure (Domec and Gartner, 2001), and 2)  $\psi_{50}$  at which hydraulic conductivity drops by about 50%, which is often used in safety-efficiency studies, is never attained in practice as  $|\psi_{50}| \gg |\psi_{l, \text{crit}}| > |\text{operating } \psi_l|$ . Atmospheric conditions and soil water states are assumed to define the prevailing conditions for all leaves and absorbing roots, respectively.

When PPFD > 0, photosynthesis commences, assimilated sugars that accumulate in the mesophyll are first transported to the companion cell and subsequently to the sieve elements in the loading zone (i.e., leaf). Loading is achieved by either active (i.e., polymer trapping and apoplastic pumping) or passive (i.e., molecular diffusion) mechanisms (Turgeon, 2010). Passive loading is common in woody seed plants (i.e., angiosperm and gymnosperm), while many herbaceous species exhibit active loading (Jensen et al., 2016; Turgeon, 2010).

At the sub-hourly time-scale defined over a fixed period  $\Delta t$ ,  $f_c(\psi_l)$ ,  $f_e(\psi_l)$ , environmental factors (e.g., atmospheric forcing and soil water status) are assumed to be stationary. Hence, over such  $\Delta t$  period, production rate of sucrose ( $P_C$ ) in the loading zone can be approximated by:

$$P_C = \frac{N_c}{\Delta t} \approx \alpha(\beta f_c A_l), \quad (6)$$

where  $N_c$  are the moles of sucrose produced in the mesophyll cells and then transported into the loading zone, and  $\alpha \in [0, 1]$  and  $\beta$  are the species-specific loading efficiency and the number of sucrose molecules produced from one assimilated  $\text{CO}_2$  molecule ( $\beta = 1/12$  for sucrose only), respectively. It must be noted that for a stationary photosynthetic rate, sucrose production (and subsequent transport) rate (i.e.,  $P_C$ ) is



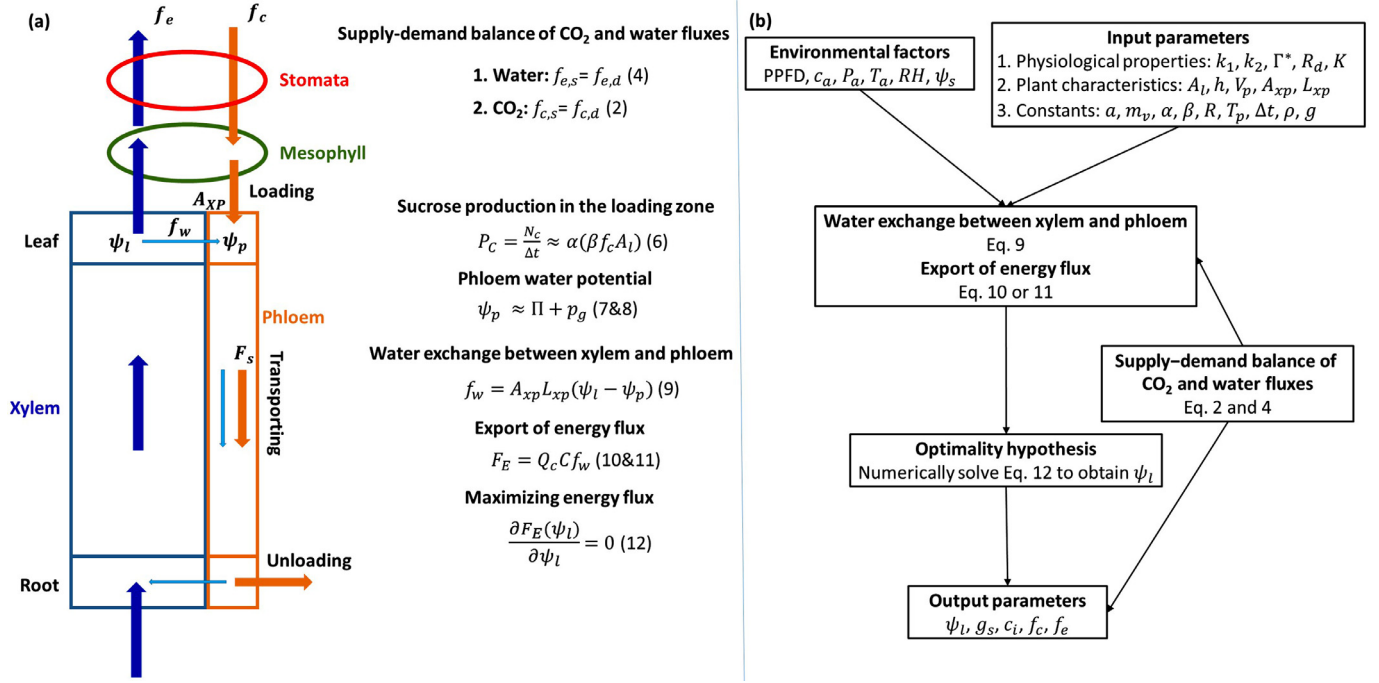


Fig. 2. (a) Schematic of the leaf-level gas exchange and the simultaneous water and sucrose mass fluxes in xylem and phloem. (b) Flowchart showing the numerical calculation process for the modeling system.

assumed to be constant. The  $\alpha$  is set to be 1 when assuming that all the sucrose molecules assimilated from  $f_c$  enter the loading zone over a  $\Delta t$  period (i.e., no time delay for different sucrose loading mechanisms) (Hölttä et al., 2017; Nikinmaa et al., 2013). The total water potential ( $\psi_p$ ) in the loading zone of the phloem includes turgor pressure ( $p_p$ ), osmotic potential ( $\Pi$ ) and gravitational potential ( $p_g = \rho gh$  where  $\rho$  is the liquid density that varies weakly with  $N_c$ ,  $g$  is the gravitational acceleration and  $h$  is the height above a datum set at the forest floor). The kinetic energy head is ignored as expected for low Reynolds number flows. Hence,

$$\psi_p = p_p + \Pi + p_g. \quad (7)$$

For an ideal solute and diluted sucrose concentration, the loading phloem sap  $\Pi$  can be computed from the van't Hoff formula (Campbell and Norman, 1998; Nobel, 2009) given by:

$$\Pi = -RT_p C, \quad (8)$$

where  $R$  is the gas constant,  $T_p$  is the absolute temperature of the loading phloem and  $C = N_c/V_p$  is the sucrose concentration accumulated over  $\Delta t$  in the loading phloem volume ( $V_p$ ). The magnitude of  $p_p$  is dictated by the elastic nature of sieve tubes and the amount of water stored in the loading phloem. That is, the relative change in  $V_p$  due to alternating shrinkage and swelling determines  $p_p$  (i.e., elastic pressure-volume curve). Over the short  $\Delta t$ , water storage in the loading phloem is also neglected and  $p_p$  may be ignored relative to  $\Pi$  (Jensen et al., 2016). The amount of water drawn from nearby xylem conduits per unit time ( $f_w$ ) is then balanced by the water outflow from the loading phloem (i.e., no water storage). The  $f_w$  is determined from the water permeability ( $L_{xp}$ ) and water potential gradient across the interface separating the xylem and phloem in the loading zone characterized by an area  $A_{xp}$  and is given by:

$$f_w = A_{xp} L_{xp} (\psi_l - \psi_p). \quad (9)$$

Thus, the export of sucrose mass ( $F_s$ ) and its associated energy flux ( $F_E$ ) driven by the accumulated sucrose molecules over a  $\Delta t$  period (i.e.,  $N_c$ ;

Eq. (6)) from the loading phloem can be determined by:

$$\begin{aligned} F_s &= C f_w, \\ F_E &= Q_C F_s, \end{aligned} \quad (10)$$

where  $Q_C$  ( $= 5637.86 \text{ kJ mol}^{-1}$ ) is the energy content of sucrose. Eq. (10) considers only advective and neglects diffusive (and dispersive) effects as well as any sucrose leaks (i.e. no loss in  $N_c$  over  $\Delta t$  in the loading phloem). Previous studies have reported that phloem sap speed mainly depends on sieve element geometry (Jensen et al., 2011; Mullendore et al., 2010) instead of plant height (i.e., the whole path of sucrose flow throughout phloem) (Dannoura et al., 2011; Liesche et al., 2015; Windt et al., 2006). Modeling analysis (Christy and Ferrier, 1973; Thompson and Holbrook, 2003) also indicated that the water influx from xylem to phloem in the leaf is the main driver responsible for sucrose transport. It is for these reasons that the aforementioned assumptions may not be too restrictive in natural settings (Jensen et al., 2016). However, it is to be noted that  $F_E$  does not represent the actual instantaneous export of energy flux. Given the steady-state assumption here,  $\Delta t$  must also be sufficiently large to allow accumulation of  $N_c$  from mesophyll cells as needed to initiate phloem transport by osmosis. After osmosis is initiated, a pulse of energy (i.e.,  $F_E$ ) occurs that then can be used to determine the optimal  $g_s$  when  $F_E$  is maximized. Residual sucrose molecules from a previous  $\Delta t$  period in the loading cell are assumed to be negligible and do not impact  $F_E$  (or  $F_s$ ). Naturally,  $\Delta t$  must also be sufficiently long to allow for the transport of sugar molecules from the mesophyll cells into the loading cell and subsequent buildup of  $N_c$  to initiate an osmo-regulated flux that exports sugars out of the loading cell. However,  $\Delta t$  must be sufficiently short so that  $f_c$  and  $g_s$  can be treated as stationary variables. Ideally, a non-steady state model that can accommodate transport processes of assimilated sugar from mesophyll to the companion cell and to the sieve elements in the leaf and to the sugar sinks (i.e., storage and unloading) throughout the plant (see Section 3.4) is required. Surrogating the effects of such unsteadiness to a pre-fixed (but constrained)  $\Delta t$  allows for the consideration of a quasi-steady model to be formulated for the instantaneous export of energy flux.

**Table 1**  
Nomenclature.

Symbol	Description	Unit
$A_l$	Leaf area	$\text{m}^2$
$A_{xp}$	Contact area between xylem and phloem in the loading zone	$\text{m}^2$
$a$	Relative diffusivity of water vapor with respect to $\text{CO}_2$	Dimensionless
$a_2$	Photosynthetic parameters ( $= K_c(1 + C_{oa}/K_o)$ )	$\mu\text{mol mol}^{-1}$
$C$	Sucrose concentration in the loading phloem	$\text{mol m}^{-3}$
$C_{oa}$	Oxygen concentration in the atmosphere	$\text{mmol mol}^{-1}$
$c_a$	Atmospheric $\text{CO}_2$ concentration	ppm
$c_i$	Inter-cellular $\text{CO}_2$ concentration	ppm
$D$	Vapor pressure deficit	kPa
$D_0$	Normalizing constant in Leuning model	kPa
$E$	Energy gain in Eq. (11)	$\text{mol s}^{-1}$
$E_c$	Limiting energy cost in Eq. (11)	$\text{mol s}^{-1}$
$E_{\max}$	Maximum permissible energy gain in Eq. (11)	$\text{mol s}^{-1}$
$F$	Reduction function BWB and LEU models	Dimensionless
$F_E$	Export of energy flux from the loading phloem	$\text{kcal s}^{-1}$
$F_s$	Export of sucrose flux from the loading phloem	$\text{mol s}^{-1}$
$F_{E, ww}$	$F_E$ under well-watered soil condition	$\text{kcal s}^{-1}$
$f_w$	Amount of water drawn from nearby xylem conduits to loading phloem per unit time	$\text{m}^3 \text{s}^{-1}$
$f_{c, d}$	Biochemical demand for $\text{CO}_2$	$\mu\text{mol m}^{-2} \text{s}^{-1}$
$f_{c, s}$	Supply of $\text{CO}_2$ flux from the atmosphere	$\mu\text{mol m}^{-2} \text{s}^{-1}$
$f_{c, \max}$	Maximum assimilation rate ( $= k_1 - R_d$ ) at $c_i \rightarrow \infty$	$\mu\text{mol m}^{-2} \text{s}^{-1}$
$f_c$	Leaf-level assimilation rate	$\mu\text{mol m}^{-2} \text{s}^{-1}$
$f_{c, \text{crit}}$	Maximum permissible assimilation rate	$\mu\text{mol m}^{-2} \text{s}^{-1}$
$f_e$	Leaf-level transpiration rate	$\text{mol m}^{-2} \text{s}^{-1}$
$f_{e, d}$	Evaporative demand	$\text{mol m}^{-2} \text{s}^{-1}$
$f_{e, s}$	Water supply function	$\text{mol m}^{-2} \text{s}^{-1}$
$f_{e, \text{crit}}$	Maximum permissible water transport capacity	$\text{mol m}^{-2} \text{s}^{-1}$
$g$	Gravitational acceleration	$\text{m s}^{-2}$
$g_s$	Stomatal conductance	$\text{mol m}^{-2} \text{s}^{-1}$
$g_{s, \text{crit}}$	Maximum permissible stomatal conductance	$\text{mol m}^{-2} \text{s}^{-1}$
$g_b$	Boundary-layer conductance	$\text{mol m}^{-2} \text{s}^{-1}$
$g_m$	Mesophyll conductance	$\text{mol m}^{-2} \text{s}^{-1}$
$g_{s, ww}$	$g_s$ under well-watered-soil condition	$\text{mol m}^{-2} \text{s}^{-1}$
$g_{s, \text{ref}}$	Referenced conductance at $D = 1$ kPa	$\text{mol m}^{-2} \text{s}^{-1}$
$H_{a, L}$	Hamiltonian for conventional SOT	$\mu\text{mol m}^{-2} \text{s}^{-1}$
$H_{a, X}$	Hamiltonian for modified SOT	$\mu\text{mol m}^{-2} \text{s}^{-1}$
$h$	Height of the leaf	m
$J$	Electron transport rate	$\mu\text{mol m}^{-2} \text{s}^{-1}$
$K$	Whole-system conductance	$\text{kg s}^{-1} \text{MPa}^{-1}$
$K_{\max}$	Maximum whole-system conductance	$\text{kg s}^{-1} \text{MPa}^{-1}$
$K_{s, \max}$	Maximum leaf-specific tree conductance ( $= K_{\max}/A_l$ )	$\text{kg s}^{-1} \text{m}^{-2} \text{MPa}^{-1}$ or $\text{mmol m}^{-2} \text{s}^{-1} \text{MPa}^{-1}$
$K_c$	Michaelis constants for $\text{CO}_2$ fixation	$\mu\text{mol mol}^{-1}$
$K_o$	Michaelis constants for oxygen inhibition	$\text{mmol mol}^{-1}$
$k_1$	Photosynthetic parameters ( $= J/4$ )	$\mu\text{mol m}^{-2} \text{s}^{-1}$
$k_2$	Photosynthetic parameters ( $= k_1 a_2/V_{c, \max}$ )	$\mu\text{mol mol}^{-1}$
$L_{xp}$	Water permeability between xylem and phloem in the loading zone	$\text{m Pa}^{-1} \text{s}^{-1}$
$m$	Stomatal sensitivity to $D$ ( $= [dg_s/d\ln(D)]/g_{s, \text{ref}}$ )	Dimensionless
$m_E$	Empirical parameter linking $g_s$ to $f_c/c_a$ in BWB and LEU models	Dimensionless
$m_v$	Molecular weight of water	$\text{kg mol}^{-1}$
$N_c$	Number of sucrose molecules	$\mu\text{mol}$
PPFD	Photosynthetically active radiation	$\mu\text{mol m}^{-2} \text{s}^{-1}$
$P$	Energy profit in Eq. 11	$\text{mol s}^{-1}$
$P_a$	Atmospheric pressure	kPa
$P_p$	Phloem turgor (or mechanical) pressure	MPa
$P_g$	Gravitational potential	MPa
$Q_c$	Energy content of sucrose	$\text{kJ mol}^{-1}$
$R$	Gas constant	$\text{J K}^{-1} \text{mol}^{-1}$
$R_d$	Daytime mitochondrial respiration rate	$\mu\text{mol m}^{-2} \text{s}^{-1}$
$RH$	Relative humidity	%
$T_a$	Air temperature	$^{\circ}\text{C}$
$T_p$	Absolute temperature of the loading phloem	K
$V_p$	Volume of loading phloem	$\text{m}^3$
$V_{c, \max}$	Maximum carboxylation capacity	$\mu\text{mol m}^{-2} \text{s}^{-1}$
$\Gamma^*$	$\text{CO}_2$ compensation point in the absence of mitochondrial respiration	$\mu\text{mol mol}^{-1}$
$\Pi$	Phloem osmotic potential	MPa
$\lambda_L$	Marginal water use efficiency for conventional SOT	$\mu\text{mol mol}^{-1}$
$\lambda_X$	Marginal water use efficiency for modified SOT	$\mu\text{mol mol}^{-1}$
$\lambda_p$	Long-term cost of maintaining transpirational stream relative to maintaining photosynthetic protein to support assimilation (Prentice et al., 2014)	$\mu\text{mol mol}^{-1}$
$\psi_l$	Leaf water potential in the xylem	MPa
$\psi_s$	Soil water potential	MPa
$\psi_p$	Total water potential in the loading phloem	MPa

(continued on next page)

Table 1 (continued)

Symbol	Description	Unit
$\psi_{l, \text{crit}}$	Leaf water potential at $f_{e, \text{crit}}$	MPa
$\psi_{12}$	Air-entry point	MPa
$\psi_{50}$	Leaf water potential at which hydraulic conductivity drops by 50%	MPa
$\alpha$	Species-specific loading efficiency ( $\in (0, 1)$ )	Dimensionless
$\beta$	Number of sucrose molecules produced from one assimilated $\text{CO}_2$ molecule ( $= 1/12$ )	Dimensionless
$\Delta t$	Hourly time scale	s
$\rho$	Liquid density in the phloem	$\text{kg m}^{-3}$

When combining Eqs. (2), (4), (6)–(10) (see Appendix A),  $F_E$  to be maximized can now be expressed as a function of  $\psi_l$  and is given as:

$$\underbrace{F_E(\psi_l)}_{\text{Energy profit (P)}} = G \left[ \underbrace{f_c^2(\psi_l)}_{\text{Energy gain (E)}} + \underbrace{I(\psi_l - p_g)f_c(\psi_l)}_{\text{Limiting cost (E}_c\text{)}} \right], \quad (11)$$

where  $G = Q_c A_{xp} L_{xp} RT_p (\alpha \beta A_l \Delta t / V_p)^2$  and  $I = (V_p / A_l) (\alpha \beta \Delta t RT_p)^{-1}$  are constants (i.e., independent of  $\psi_l$ ) associated with phloem system properties. The  $F_E$  here has a unit of joule per time and represents the energy profit due to the addition of sucrose molecules arising from  $f_c^2$  supplied by the atmosphere over a  $\Delta t$  period. The first term on the right-hand side represents the energy gain ( $E = f_c^2(\psi_l)$ ) but is constrained by the soil-xylem hydraulic system for a given  $\psi_s$  (see Eqs. (2) and (4)). This constraint arises because the solutions of  $\partial f_c / \partial g_s \times \partial g_s / \partial \psi_l = 0$  and  $\partial f_e / \partial g_s \times \partial g_s / \partial \psi_l = 0$  are the same. As  $\psi_l$  decreases with increasing  $g_s$ , a larger energy gain is achieved until the maximum permissible energy gain ( $E = E_{\text{max}}$ ) is reached at  $\psi_{l, \text{crit}}$ . However, the decrease in  $\psi_l$  also impedes  $f_w$  that drives  $F_E$  (see Eqs. (9) and (10)). This mechanism, which represents an additional cost of energy ( $E_c$ ) due to interaction between xylem and phloem in the loading leaf, is the physical significance of the second term on the right-hand side of Eq. (11). The  $E_c$  is always a cost term because the value of  $(\psi_l - p_g)$  is never positive. When the drop in  $\psi_l$  reaches a certain threshold ( $\psi_{l, \text{opt}}$ ) expected to occur before  $\psi_{l, \text{crit}}$ , the increase in energy gain is no longer larger than the increase in the limiting cost, implying diminishing returns of energy profit ( $P$ ) in the system. The optimal  $\psi_{l, \text{opt}}$  that ensures a maximum  $P$  (i.e.,  $F_E$ ) can now be determined by setting

$$\frac{\partial F_E(\psi_l)}{\partial \psi_l} = 0, \quad (12)$$

when  $\partial^2 F_E(\psi_l) / \partial \psi_l^2 < 0$ . As shown in Fig. 2(b),  $\psi_{l, \text{opt}}$  (i.e., operating  $\psi_l$ ) is numerically solved through Eq. (12) for a given set of environmental factors, physiological properties, plant characteristics and constant parameters. The corresponding  $g_s$ ,  $c_v$ ,  $f_c$  and  $f_e$  can be computed from Eqs. (2) and (4). Eq. (12) sets the optimal criterion that reflects the energetics of the evolution principle (Lotka, 1922), in which the energy flux is maintained efficient (maximum) at current state when the system is explicitly subjected to the limiting constraints through the transport or physiological processes. A favorable plant body that can enhance larger energy flux through the system may be further promoted by the maximum input of energy flux. The points of departure from the conventional SOT or profit-maximization are that (1) the *Gain* in the objective function here is proportional to  $f_c^2$  (not  $f_c$ ); and (2) the *Cost* is directly derived (not externally assumed) from the limiting constraints imposed on the system and arises from xylem-leaf-phloem interaction. In the present modeling framework, however, a number of mechanisms (e.g., adjustments in mesophyll conductance and osmotic regulation with different soil water status) that may potentially impact the transport system and subsequently the *Gain* and *Cost* are not considered but discussed later in Section 3.4. We now show that the proposed approach recovers the form of objective function (i.e., *Gain-Cost* where *Gain* and *Cost* are linearly proportional to  $f_c$  and  $f_e$  or a function of  $\psi_l$ , respectively) in the conven-

tional SOT and profit-maximization that predict  $g_s$  for well-watered soil condition.

## 2.2. Recovery of prior formulations for well-watered soil conditions

Because prior  $g_s$  formulations have been shown to describe a large corpus of data (especially under well-watered conditions), it is assumed that their mathematical form offers a compact representation of all such experiments. When the soil moisture content is near saturation (i.e.,  $|\psi_s| < |\psi_l|$ ) and the operating  $|\psi_l|$  for plants shorter than c. 20 m is much larger than  $p_g$  at high  $f_e$  (Manzoni et al., 2013a), Eq. (11) can be further simplified to (see Appendix A)

$$F_{E, \text{ww}}(\psi_l) = G \left[ f_c^2(\psi_l) - m_v I A_l \frac{f_e(\psi_l)}{K(\psi_l)} f_c(\psi_l) \right], \quad (13)$$

where the energy profit  $F_{E, \text{ww}}$  is defined for well-watered conditions. Again, the optimal  $\psi_{l, \text{opt}}$  can be obtained by setting  $\partial F_{E, \text{ww}} / \partial \psi_l = 0$  that then yields:

$$\frac{\partial f_c(\psi_l)}{\partial \psi_l} - \frac{m_v I A_l}{2} \left[ \underbrace{\frac{f_e(\psi_l)}{K(\psi_l) f_c(\psi_l)} \frac{\partial f_c(\psi_l)}{\partial \psi_l}}_M + \underbrace{\frac{\partial}{\partial \psi_l} \left( \frac{f_e(\psi_l)}{K(\psi_l)} \right)}_N \right] = 0. \quad (14)$$

A scaling analysis featured in Appendix B compares the two contributions, labeled M and N, in Eq. (14). The outcome of this analysis shows smaller contribution of term M when compared with term N. This finding may have been anticipated for well-watered soil conditions because the reduction in  $K$  is usually small at  $\psi_s \approx 0$  when stomatal closure commonly occurs before the air-entry point (i.e., at  $\psi_l$  where 12% of  $K$  losses occur) (Bond and Kavanagh, 1999; Sparks and Black, 1999). Based on this scaling analysis, Eq. (14) can be further simplified to:

$$\frac{\partial}{\partial \psi_l} \left[ f_c(\psi_l) + \frac{I}{2} \psi_l \right] = 0, \quad (15)$$

or

$$\frac{\partial}{\partial \psi_l} \left[ f_c(\psi_l) - \underbrace{\frac{V_p m_v}{2 \alpha \beta K_{\text{max}} \Delta t R T_p}}_{\lambda_x} f_e(\psi_l) \right] = 0. \quad (16)$$

Interestingly, Eqs. (15) and (16) converge respectively to the profit-maximization (Wolf et al., 2016) and to the modified SOT (Eq. (5)). This convergence suggests a tight connection between the leaf-xylem-phloem system given the **dissimilarity** in objective functions. The emergence of a linear relation between  $g_s$  and  $\psi_l$  for a nearly constant  $K_{\text{max}}$  at  $\psi_s \approx 0$  (see Eq. (4)) also results in the convergence of the conventional and modified SOT's:  $\partial H_{a, L}(g_s) / \partial g_s = 0$  is equivalent to  $\partial H_{a, X}(\psi_l) / \partial \psi_l = 0$  and  $\lambda_L = \lambda_X$ . One of the main novelties here is the predicted dependency of  $\lambda_X$  (or  $\lambda_L$ ) on xylem and phloem properties arising from the condition  $\partial F_{E, \text{ww}} / \partial \psi_l = 0$ . The analysis may also indicate why the time-scale used for SOT to predict  $g_s$  remains uncertain (Buckley et al., 2016). Current uncertainty in determining  $\lambda_X$  arises from the inexact specification of  $\Delta t$ . Again, a non-steady state model is needed to eliminate the dependency of  $\lambda_X$  (or  $\lambda_L$ ) on  $\Delta t$ .

An analytical solution for the proposed approach (i.e., Eq. (16)) can now be derived under some conditions. Assuming  $f_c \gg R_d$ ,  $c_i \gg \Gamma^*$ , the optimal  $g_s$  and  $c_i/c_a$  are given as (see Appendix C):

$$g_{s,ww} = \left(1 + \sqrt{\frac{k_2 + \Gamma^*}{aD\lambda_X}}\right) \frac{f_c}{c_a},$$

$$\frac{c_i}{c_a} = \frac{\sqrt{\frac{k_2 + \Gamma^*}{a\lambda_X}}}{\sqrt{\frac{k_2 + \Gamma^*}{a\lambda_X}} + \sqrt{D}}. \quad (17)$$

The link between the xylem, phloem, and leaf is provided here by  $\lambda_X$  (see Eq. (16)). When  $f_c$  operates under RuBP limitation, Eq. (17) converges to the form of  $g_s$  derived from conventional SOT proposed elsewhere (Medlyn et al., 2011). If the higher order terms in the Taylor series expansion expressing  $c_i/c_a$  are neglected, as shown in Appendix C, the optimal  $g_s$  and  $c_i/c_a$  simplify to:

$$g_{s,ww} = \sqrt{\frac{k_2 + \Gamma^*}{a\lambda_X}} \frac{f_c}{c_a} D^{-1/2},$$

$$\frac{c_i}{c_a} = 1 - \sqrt{\frac{a\lambda_X}{k_2 + \Gamma^*}} \sqrt{D}. \quad (18)$$

Eq. 18 also recovers the linear dependency of  $g_s$  on  $f_c/c_a$  as in BWB and LEU models and suggests that  $m_E$  encodes the xylem-phloem system properties. Also, the predicted  $c_i/c_a$  varies marginally with  $D$  as has been known for some time now (Wong et al., 1979). Eq. (18) also recovers the form of optimal  $g_s$  and  $c_i/c_a$  derived by others (Katul et al., 2010; 2012; Volpe et al., 2011) when a linearized biochemical demand function is assumed (as expected for Rubisco limitations on  $f_c$ ). The convergence of analytical solutions here can be expected when they are all derived from the same objective function (i.e., Eq. (16)) for well-watered condition. These analytical solutions mainly differ in the choice of RuBP or Rubisco limitations (i.e., limitation regime is known) on  $f_c$  that can be bypassed when co-limitation (i.e., Eq. (1)) is accounted for (Vico et al., 2013). Neglecting  $\Gamma^*$  and  $R_d$  may generate unrealistic  $g_s$  responses at low  $c_a$  although this assumption may not be too restrictive especially when  $c_a$  is expected to increase above current level (i.e., > 400 ppm). However, these analytical solutions are invalid under water stress condition unless variations in  $\lambda_X$  with  $\psi_s$  can be appropriately described (Manzoni et al., 2011).

As suggested elsewhere (Prentice et al., 2014), the optimal  $g_s$  and  $c_i/c_a$  under Rubisco-limitation can be assumed to operate with minimum maintenance cost that simultaneously maximizes  $f_c$  and  $f_e$  and are given as:

$$g_{s,ww} = \left(1 + \sqrt{\frac{a_2}{aD\lambda_p}}\right) \frac{f_c}{c_a},$$

$$\frac{c_i}{c_a} = \frac{1}{1 + \sqrt{\frac{a\lambda_p}{a_2}} \sqrt{D}}, \quad (19)$$

where  $\lambda_p$  is the long-term cost of maintaining transpirational stream relative to maintaining photosynthetic protein to support assimilation. Again, the current approach recovers similar forms of  $g_s$  and  $c_i/c_a$  to Eq. (19) and the dependency of the apparent  $\lambda_p$  on  $K_{\max}^{-1}$  is also reflected by  $\lambda_X$  analytically derived here. This dependency of  $\lambda_X$  on  $K_{\max}^{-1}$  has been inferred by fitting SOT to a numerical model with consideration of whole-plant sucrose transporting length (Hölttä et al., 2017). The effects of drying soil process on  $g_s$  is embedded in  $a/b$  ( $= \lambda_p \sim K^{-1}$ ) in Prentice et al. (2014) that is equivalent to  $\lambda_X$  in SOT while the increase

**Table 2**

Physical characteristics of needle samples adopted elsewhere (Domec et al., 2016b) and anatomical attributes of phloem for the loading leaf of *Pinus taeda* L. growing under ambient- $^{a}\text{CO}_2$  and elevated- $^{c}\text{CO}_2$  conditions at Duke-FACE site.

	$A_n$ (mm <sup>2</sup> )	$L_n$ (cm)	$d_p$ (μm)	$N_p$
$^{a}\text{CO}_2$	0.50	17.4	5.75	330
$^{c}\text{CO}_2$	0.48	18.0	5.58	276

$A_n$ : needle cross-sectional area;  $L_n$ : needle length;  $d_p$ : diameter of phloem cell;  $N_p$ : number of phloem cells per needle.

in the carbon cost represented as a function of  $\psi_l$  (i.e.,  $\theta(\psi_l)$ ) with decreasing  $\psi_l$  is assumed in Wolf et al. (2016). The modeling approaches proposed by Prentice et al. (2014) and Wolf et al. (2016) can accommodate how  $g_s$  is impacted by the reduction in  $K$  as drought progresses but may not reflect the isohydric-to-anisohydric behavior that can be explained by the energy partitioning between  $P$ ,  $E$  and  $E_c$  in Eq. (11) (see Section 3.2). In the absence of drought stress, the convergence of various optimization goals shown here invites the use of the energetics of the evolution principle as a unifying hypothesis to predict  $g_s$ .

### 3. Results and discussion

To address the study objectives, we first analyze how different transport and physiological processes impact the short-term  $g_s$  responses to environmental factors through model calculations featured in Section 3.1. In particular, we first examine the sensitivity of  $g_s$  to  $D$  and  $\psi_l$  that has been well documented in the literature. In Section 3.2, we then explore how the difference in the coordinated leaf-xylem-phloem system determines different water use strategies among plants (i.e., isohydric-to-anisohydric behavior) during a soil dry-down process. The analysis here is accomplished by examining how the difference in the soil-xylem hydraulics impact the energy partitioning in Eq. (11) (i.e.,  $P$ ,  $E$  and  $E_c$ ) and hence the sensitivity of  $\psi_l$  to  $\psi_s$  and  $D$ . We also explain the general decreasing trends in  $g_s$  following elevated atmospheric  $\text{CO}_2$  concentration sustained over long time-scales in Section 3.3. Specifically, how the adjustments in plant hydraulic and physiological properties in response to a new stationary  $\text{CO}_2$  concentration level modify the value of  $\lambda_X$  dictating leaf-level gas exchange is explored. Finally, we briefly summarize the study limitation in the present modeling framework in Section 3.4. For all the following model calculations (i.e., model base case), the physiological, hydraulic and allometric attributes of soil-plant system for coniferous species in general reported elsewhere (Huang et al., 2017) are adopted. Physical characteristics of leaves and anatomical attributes of phloem for *Pinus taeda* L. listed in Table 2 are used.

#### 3.1. Stomatal responses to variations in environmental conditions

To illustrate a number of features of the new  $g_s$  model, the focus now is on  $g_s$  responses to short-term (sub-daily) variations in environmental factors. It is assumed that at sub-daily time-scales, the hydraulic and physiological properties of plants remain constant. The proposed approach to  $g_s$  captures the main features of stomatal responses to key environmental factors including PPFD,  $c_a$ ,  $D$ ,  $T_a$  and  $\psi_s$  (Fig. 3). The overall negative trends in  $g_s$  with respect to increasing  $D$  (Aphalo and Jarvis, 1991; Ball and Farquhar, 1984; Farquhar et al., 1980a; Grantz, 1990; Katul et al., 2009; Lange et al., 1971; Lendzion and Leuschner, 2008; Massman and Kaufmann, 1991; McAdam and Brodribb, 2015; Monteith, 1995; Morison and Gifford, 1983; Oren et al., 1999; Schulze et al., 1974) and decreasing  $\psi_s$  (Berninger et al., 1996) are governed by the supply-demand balance of water flux (i.e., Eq. (4)) that presets the maximum permissible stomatal conductance ( $g_{s, \text{crit}}$ ) and subsequently  $E_{\max}$  in Eq. (11) at  $\psi_l, \text{crit}$ . To examine the sensitivity of predicted  $g_s$  to  $D$ , the empirical relation between  $g_s$  and  $D$  (Oren et al., 1999) is adopted



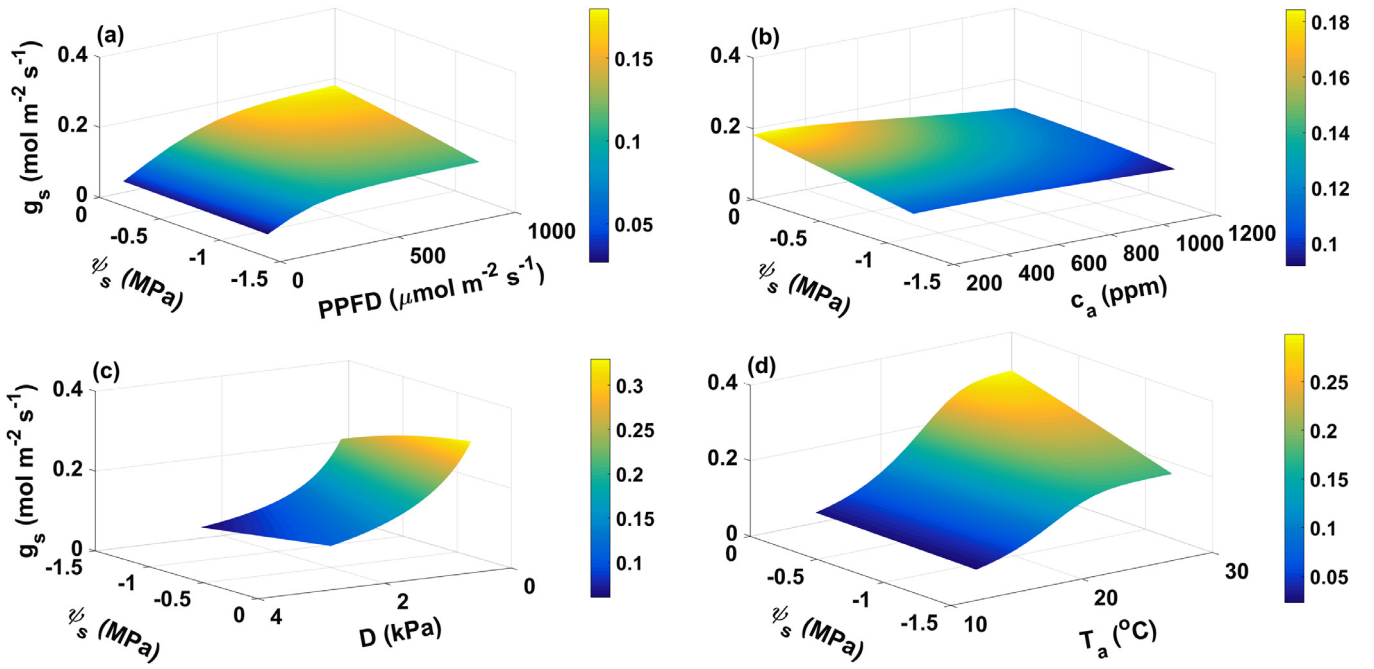


Fig. 3. Modeled stomatal conductance ( $g_s$ ) as a function of soil water potential ( $\psi_s$ ) and (a) photosynthetically active radiation (PPFD), (b) atmospheric  $\text{CO}_2$  concentration ( $c_a$ ), (c) vapor pressure deficit ( $D$ ) and (d) air temperature ( $T_a$ ). All the model parameters used here are the same as Fig. 1. PPFD,  $T_a$ ,  $c_a$  and  $RH$  are respectively fixed to be  $1000 \mu\text{mol m}^{-2} \text{s}^{-1}$ ,  $25^\circ\text{C}$ ,  $400 \text{ ppm}$  and  $50\%$  in general while PPFD varies from  $100$  to  $1000 \mu\text{mol m}^{-2} \text{s}^{-1}$  in (a),  $c_a$  varies from  $200$  to  $1200 \text{ ppm}$  in (b),  $RH$  varies from  $10$  to  $80\%$  in (c), and  $T_a$  varies from  $15$  to  $30^\circ\text{C}$  with a fixed  $D = 1 \text{ kPa}$ .

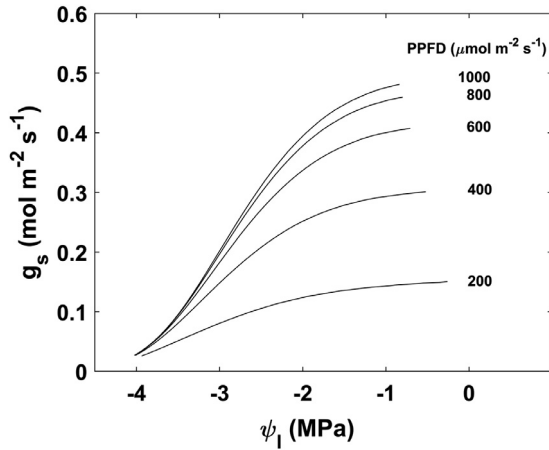


Fig. 4. Modeled stomatal conductance ( $g_s$ ) as a function of leaf water potential ( $\psi_l$ ) for different photosynthetically active radiation (PPFD) with a range from  $200$  to  $1000 \mu\text{mol m}^{-2} \text{s}^{-1}$ . All the model parameters used here are the same as Fig. 1. The air temperature ( $T_a$ ), atmospheric  $\text{CO}_2$  concentration ( $c_a$ ) and relative humidity ( $RH$ ) are respectively set to be  $25^\circ\text{C}$ ,  $400 \text{ ppm}$  and  $90\%$ .

as it encodes a large corpus of leaf and sapflow data. This expression is given as:

$$g_s = g_{s,ref} [1 - m \times \ln(D)], \quad (20)$$

where  $g_{s,ref}$  is the reference conductance at  $D = 1 \text{ kPa}$  and  $m$  is the ratio of  $dg_s/d\ln(D)$  to  $g_{s,ref}$ . Using all the model runs in Fig. 3(c), the value of  $m$  determined by least-square fit to Eq. (20) is  $0.61$  and is close to the value (i.e.,  $0.59$ ) derived from a meta-analysis of c. 30 species (Oren et al., 1999). When  $\psi_s$  decreases, the predicted relation between  $g_s$  and  $\psi_l$  (Fig. 4) also recovers a Weibull-type form that has been globally observed (Klein, 2014). This Weibull-type  $g_s - \psi_l$  relation is mainly dictated by the shape of  $K(\psi_l)$  (i.e., soil-xylem hydraulics) without relying on a pre-specified  $\psi_l$ -dependent  $\lambda_X$  (Manzoni et al., 2011) or any cost

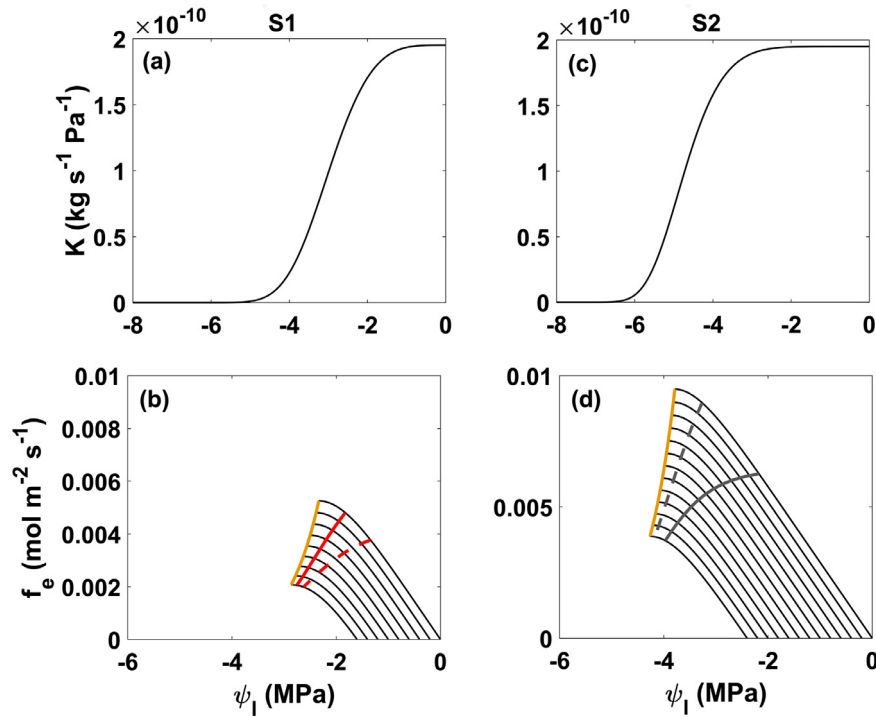
function linked with xylem hydraulics (Wolf et al., 2016) formulated in SOT or profit-maximization. The predicted  $c_i/c_a = 0.82 \pm 9.8\%$  across all runs for well-watered soil condition in Fig. 3, representing a relatively conservative  $c_i/c_a$  when compared with  $g_s$ ,  $f_c$ ,  $f_e$  and  $\psi_l$ . This predicted near-constant  $c_i/c_a$  is supported by previous studies ( $c_i/c_a = 0.6 - 0.9$ ) (Drake et al., 1997; Ehleringer and Cerling, 1995; Prentice et al., 2014; Wong et al., 1979). Based on a constant  $c_i/c_a$ , the general trends in negative stomatal response to  $c_a$  (Mansfield et al., 1990; Messinger et al., 2006; Morison, 1998; Morison and Gifford, 1983; Mott, 1988) and positive stomatal response to PPFD and  $T_a$  (Schulze et al., 1974; Wong et al., 1979) are mainly reflected by the supply-demand balance of  $\text{CO}_2$  flux.

### 3.2. Coordinated photosynthetic-hydraulic-sucrose transporting machinery explaining isohydric-to-anisohydric behavior

The analysis is now expanded to examine the coordinated photosynthetic-hydraulic-sucrose transporting machinery in species with different water use strategies across the spectrum of isohydric-to-anisohydric behavior as drought progresses.

#### 3.2.1. General features of isohydric-to-anisohydric behavior and the model set-up

The isohydric-to-anisohydric behavior is mainly defined by the sensitivity of  $\psi_l$  to  $\psi_s$  and  $D$  (Martínez-Vilalta and García-Forner, 2017). The general features differentiating isohydric and anisohydric behavior (Domec and Johnson, 2012; Meinzer et al., 2016) are that (1) isohydric species tend to maintain a relatively constant midday  $\psi_l$  that is less sensitive to decreasing  $\psi_s$  and increasing  $D$ ; (2) anisohydric species allow midday  $\psi_l$  to significantly decrease with decreasing  $\psi_s$  and increasing  $D$  such that a relatively larger  $f_e$  and  $f_c$  can be maintained when compared to isohydric species. Studies conducted to contrast isohydric and anisohydric behavior (Kolb and Sperry, 1999; McDowell et al., 2008; Schultz, 2003; Sperry et al., 1998; 2002) reported that species with larger  $\psi_{12}$  (i.e., air-entry point that is commonly defined at  $\psi_l$  where  $12\%$  of  $K$  losses occur) tend to exhibit more isohydric behavior while anisohydric behavior occurs in species with a smaller  $\psi_{12}$ . The proposed model is



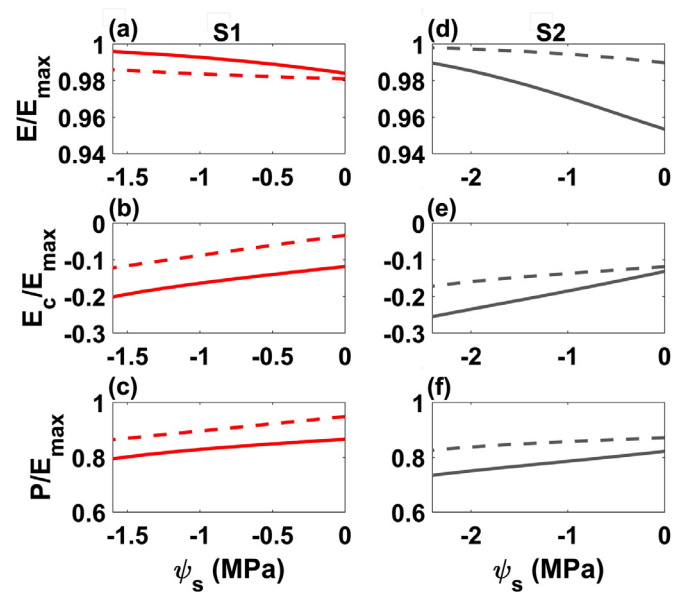
**Fig. 5.** (a) Whole-system hydraulic conductance ( $K$ ) as a function of total leaf water potential ( $\psi_l$ ) for scenario 1 (S1). (b) Water supply function for S1 determined by  $K$  and  $\psi_l$  for different soil water potential ( $\psi_s$ ) with maximum permissible transpiration rate ( $f_{e, \text{crit}}$ ; orange solid line) and predicted transpiration rate ( $f_e$ ; red solid line). All the model parameters used in (a) and (b) are the same as Fig. 1. The photosynthetically active radiation (PPFD), air temperature ( $T_a$ ), atmospheric  $\text{CO}_2$  concentration ( $c_a$ ) and relative humidity ( $RH$ ) are respectively set to be  $1200 \mu\text{mol m}^{-2} \text{s}^{-1}$ ,  $25^\circ \text{C}$ ,  $400 \text{ ppm}$  and  $50\%$ . The range of  $\psi_s$  is from  $0$  to  $-1.6 \text{ MPa}$ . For S1, the predicted  $f_e$  with  $RH = 80\%$  is shown (red dashed line). (c) and (d) are the same as (a) and (b) but for a smaller air-entry point ( $\psi_{12}$ ) where a nearly constant maximum conductance ( $K_{\text{max}}$ ) can operate represented as scenario 2 (S2). The range of  $\psi_s$  is from  $0$  to  $-2.4 \text{ MPa}$ .  $f_{e, \text{crit}}$  and predicted  $f_e$  in S2 are respectively represented by orange and gray solid lines. For S2, the predicted  $f_e$  with  $50\%$  increases in maximum carboxylation capacity and light saturated rate of electron transport is shown (gray dashed line). (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

now shown to be able to reconcile connections between  $\psi_{12}$  and the defining features of isohydric-to-anisohydric.

For this reason, two scenarios (S1 with larger  $\psi_{12}$  and S2 with smaller  $\psi_{12}$ ) are now constructed to illustrate how the magnitude of  $\psi_{12}$  modifies the leaf-xylem-phloem system and impacts isohydric-to-anisohydric behavior during reduced soil moisture conditions (Fig. 5). All the model parameters used for S1 are the same as the model base case. A smaller  $\psi_{12}$  is selected for S2 but all other model parameters are maintained the same as S1. The plant hydraulic and physiological properties are assumed to be constant (i.e., no acclimation or adaptation) during a soil dry-down process. The environmental factors (i.e., PPFD,  $T_a$ ,  $c_a$ ,  $RH$  and  $\psi_s$ ) used in the model runs are maintained the same for S1 and S2. The model results (i.e., predicted  $f_e$ ,  $E/E_{\text{max}}$ ,  $E_c/E_{\text{max}}$  and  $P/E_{\text{max}}$ ) for the two cases are respectively represented as red and gray solid lines for S1 and S2 in Figs. 5 and 6. For S1, a larger  $RH$  is also used in another model run to examine if a reduced  $D$  can modify isohydric-to-anisohydric behavior, as represented by red dashed lines in Figs. 5 and 6. For S2, we also use a larger photosynthetic capacity (i.e., larger  $k_1$  and  $k_2$ ) to explore the effects of relative magnitude of photosynthetic capacity in relation to the water transport capacity on the isohydric-to-anisohydric behavior, as represented by gray dashed lines in Figs. 5 and 6. Specifically, it is shown that maximizing the energy profit  $P$  across these two different  $\psi_{12}$  scenarios recovers the key features delineating isohydric from anisohydric behavior. For simplicity, it is assumed that  $K_{\text{max}}$  maintains a near-constant value as loss of conductivity at  $\psi_{12}$  is assumed to be minor ( $\sim 12\%$ ).

### 3.2.2. Linkage between the energy partitioning in Eq. (11) and the sensitivity of $f_e$ and $\psi_l$ to $\psi_s$ and $D$

As  $g_s$  increases monotonically with decreasing  $\psi_l$  (up to  $\psi_{l, \text{crit}}$ ),  $E_{\text{max}}$  occurs at  $f_{e, \text{crit}}$  and can be surrogated to a preset  $f_{e, \text{crit}}$  for a given  $\psi_s$ .



**Fig. 6.** The energy partitioning in Eq. (11) for the two scenarios (S1 and S2). The energy gain ( $E$ ), limiting cost ( $E_c$ ) and energy profit ( $P$ ) relative to maximum permissible energy gain ( $E_{\text{max}}$ ) as a function of soil water potential ( $\psi_s$ ) are respectively shown in (a), (b) and (c) for S1. The model results for  $RH = 50\%$  and  $80\%$  are respectively represented by the red solid and dashed lines. (d), (e) and (f) are the same as (a), (b) and (c) but for S2. Same as Fig. 5(d), model results for  $50\%$  increases in maximum carboxylation capacity and light saturated rate of electron transport are represented by gray dashed lines. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

The  $E_{\max}$  is constrained by the soil-xylem limitation (see Eq. (11) and Section 1.2). However, the corresponding  $\psi_{l, \text{crit}}$  does not guarantee a maximum  $P$  due to finite  $E_c$  as discussed in Section 2.1. In Eq. (11), maximum  $P$  occurs at  $\psi_{l, \text{opt}} (> \psi_{l, \text{crit}})$  and the corresponding predicted  $f_e$  or  $f_c$  can be used as an indicator for the actual level of  $E$ . Thus, the energy partitioning between  $P$ ,  $E$  and  $E_c$  in Eq. (11) (Fig. 6) can be used to explain the sensitivity of  $f_e$  and  $\psi_l$  to  $\psi_s$  and  $D$  that then determines isohydric-to-anisohydric behavior.

### 3.2.3. Similar behavior of isohydric and anisohydric plants under severe drought condition

The common feature of the two scenarios is that the difference between  $f_{e, \text{crit}}$  (i.e., orange lines in Fig. 5(b) and (d)) and predicted  $f_e$  ( $\Delta f_e$ ) decreases as drought progresses. This decreasing trend in  $\Delta f_e$  is reflected by the increasing trend in  $E/E_{\max}$  up to nearly unity, implying that soil-xylem limitation dominates  $P$  at a small  $\psi_s$ . However,  $\partial(E/E_{\max})/\partial\psi_s < 0$  does not suggest that  $E$  is enhanced by a smaller  $\psi_s$ . As  $\psi_s$  drops, the decrease in  $E$  ( $\sim f_c^2$ ) is smaller than the decrease in  $E_{\max}$  ( $\sim f_{c, \text{crit}}^2$ ) but  $P$  can be further suppressed by increasing  $E_c$  when severe drought conditions persist.

### 3.2.4. Isohydric and anisohydric behavior

When compared with S1, a smaller  $\psi_{12}$  in S2 allows a more negative operating  $\psi_l$  (i.e., anisohydric behavior) that further enhances the impediment of sucrose transport (i.e.,  $E_c$ ). The smaller  $E/E_{\max}$  in the case of S2 also suggests that the maximum permissible water transport capacity (i.e.,  $f_{e, \text{crit}}$ ) significantly overshoots the actual  $f_e$  required to attain the maximum  $P$  especially when  $\psi_s \rightarrow 0$ . This over-built soil-xylem hydraulics in S2 also permits a broader operating range of  $\psi_l$  in response to environmental factors such as  $D$ , PPFD and  $T_a$ . In the absence of water stress, it is advantageous to maintain maximum  $P$  and a larger  $f_c$  ( $< f_{c, \text{crit}}$ ) although a larger  $f_e$  can be achieved by changes in environmental conditions (i.e., increasing  $D$ , PPFD or  $T_a$ ). When compared with S2,  $\Delta f_e$  in the case of S1 is smaller due to a larger  $\psi_{12}$  (i.e., isohydric behavior; a narrower range of  $\psi_l$  where a nearly constant  $K_{\max}$  can operate). It is suggested that the main limiting component is the soil-xylem hydraulics, leading to smaller  $E_c$  and larger  $E/E_{\max}$  in S1. Although the maximum  $P$ ,  $E_{\max}$  ( $\sim f_{c, \text{crit}}^2$ ) and operating  $E$  ( $\sim f_c^2$ ) in S1 are suppressed by a larger  $\psi_{12}$ , the limitation induced by the interaction between xylem and phloem in the loading leaf (i.e.,  $E_c$ ) is also reduced due to a larger operating  $\psi_l$ . However, if  $D$  in the case of S1 is reduced, the decrease in  $f_e$  (i.e., increase in  $\psi_l$ ) results in a larger  $\Delta f_e$  (Fig. 5(b)) and smaller  $E/E_{\max}$  (Fig. 6(a)) where the enhancement in  $E_{\max}$  is larger than the enhancement in  $E$ . A reduced  $D$  also suppresses  $E_c$  due to the increase in  $\psi_l$ . This finding suggests that the maximum  $P$  and operating  $E$  can be enhanced even when the range of  $\psi_l$  is small (i.e., a larger  $\psi_{12}$ ) for a nearly constant  $K_{\max}$ . Similar to S2,  $\psi_l$  in S1 can now respond to a wider range of  $D$  at short time-scale as a consequence of reduced  $f_e$ .

Hence, S1 and S2 may represent plant hydraulics associated with the more conservative and aggressive water use strategies for plants across the spectrum of isohydric-to-anisohydric behavior. However, the range of  $\psi_l$  for a nearly constant  $K_{\max}$  to operate (i.e.,  $\psi_{12}$ ) alone cannot be used to differentiate species with different water use strategy. To illustrate,  $\Delta f_e$  decreases with increasing photosynthetic capacity (i.e., larger  $k_1$  and  $k_2$  are used in S2), leading to a shift from anisohydric to isohydric behavior (i.e., narrower range of operating  $\psi_l$  along the gray dashed line) as shown in Fig. 5(d). A larger photosynthetic capacity also necessitates a larger  $f_e$  that reduces  $\Delta f_e$  and increases  $E/E_{\max}$  because soil-xylem hydraulics now dominate with a reduced contribution of  $E_c$  to  $P$  (gray dashed lines in Fig. 6(d), (e) and (f)).

To sum up, it is fair to state that the photosynthetic capacity for isohydric species has the tendency to nearly exploit  $f_{e, \text{crit}}$  throughout a dry-down (i.e.,  $E/E_{\max} \rightarrow 1$ ). Isohydric plants are conservative water users (i.e., limited by soil-xylem hydraulics) but their photosynthetic capacity is aggressively utilizing the soil-xylem hydraulic system. Anisohydric plants, by contrast, are aggressive water users but they adopt

more conservative photosynthetic capacity that requires smaller  $f_e$  to maintain a maximum  $P$  compared to their  $f_{e, \text{crit}}$  state. When responding to fluctuation in environmental conditions, the compartments of the system appear to operate in a *coordinated* manner so as to maintain  $P/E_{\max}$  without any apparent bottleneck even when  $\psi_s$  drops. While previous experimental studies mainly focused on the variation of  $\psi_l$  during a dry-down and the sensitivity of  $g_s$  to  $D$  and  $\psi_s$  to distinguish isohydric-to-anisohydric behavior (Domec and Johnson, 2012; Meinzer et al., 2016), the finding here forms a new model-generated hypothesis that has not been explored and requires testing in future field and laboratory experiments. That is, the magnitude of atmospheric aridity (i.e.,  $D$ ) and the relative magnitude of photosynthetic capacity in relation to the water transport capacity through soil-xylem hydraulic system can shift isohydric-to-anisohydric behavior.

### 3.3. Long-term effect of elevated atmospheric $\text{CO}_2$ concentration on leaf-level gas exchange

When plants acclimate or adapt to a changing environment, leaf-level gas exchange reflects concomitant adjustments in plant hydraulic and physiological properties. Under well-watered soil conditions, the closed form expressions for  $g_{s, \text{ww}}$ ,  $f_c$  and water use efficiency ( $\text{WUE} = f_c/f_e$ ) can be derived by replacing Eq. (17) into the supply-demand balance of  $\text{CO}_2$  flux, and are given as:

$$\begin{aligned} g_{s, \text{ww}} &= \frac{k_1 \left( 1 + \sqrt{\frac{k_2 + \Gamma^*}{aD\lambda_X}} \right)}{k_2 \left( 1 + \sqrt{\frac{aD\lambda_X}{k_2 + \Gamma^*}} \right) + c_a}, \\ f_c &= \frac{k_1 c_a}{k_2 \left( 1 + \sqrt{\frac{aD\lambda_X}{k_2 + \Gamma^*}} \right) + c_a}, \\ \text{WUE} &= \frac{c_a/aD}{1 + \sqrt{\frac{k_2 + \Gamma^*}{aD\lambda_X}}}. \end{aligned} \quad (21)$$

On long time-scales, xylem and phloem traits (i.e.,  $\lambda_X$ ) and photosynthetic parameters (i.e.,  $k_1$  and  $k_2$ ) in Eq. (21) are shaped by the environmental conditions they have experienced. However,  $g_{s, \text{ww}}$ ,  $f_c$ ,  $\text{WUE}$  and  $c_i/c_a$  (i.e., Eq. (17)) represent short-term leaf-level responses to current states or environmental conditions. A large time-scale separation exists between variations in endogenous plant attributes (encoded in  $\lambda_X$ ,  $k_1$  and  $k_2$ ) and instantaneous leaf-level responses (i.e.,  $g_{s, \text{ww}}$ ,  $f_c$ ,  $\text{WUE}$  and  $c_i/c_a$ ). For this reason, Eqs. (21) and (17) only focus on how measured modifications in  $\lambda_X$  following long-term elevated atmospheric  $\text{CO}_2$  concentration modify photosynthetic parameters as well as  $g_{s, \text{ww}}$ ,  $c_i/c_a$  ratio,  $f_c$  and  $\text{WUE}$ . For simplicity, the focus is on formulations that assume absence of water stress after the plants experience different  $c_a$ 's on long time-scales (e.g., by comparing leaves grown under ambient and enriched  $c_a$  conditions). Such a situation describes the setup for *Pinus taeda* L. growing under +200 ppm  $\text{CO}_2$  above current level as reported from the Duke-Free Air  $\text{CO}_2$  Enrichment (FACE) site. The Duke-FACE was conducted in a South-Eastern U.S. pine forest (Domec et al., 2009; 2016b; Tor-ngern et al., 2015) where leaf and plant hydraulic traits have been measured. When other environmental conditions are maintained the same, a reduced maximum leaf hydraulic conductance ( $K_{\text{leaf, max}}$ ) was reported with increased  $c_a$ . In this case, the maximum leaf-specific tree conductance ( $K_{s, \text{max}} = K_{\text{leaf, max}}/A_l$ ) decreased from 0.65 to 0.43  $\text{mmol m}^{-2} \text{s}^{-1} \text{MPa}^{-1}$  (Domec et al., 2016a) as a result of the reduction in  $K_{\text{leaf, max}}$  (Domec et al., 2009). This general decrease in  $K_{s, \text{max}}$  has been reported for ring-porous, diffuse-porous, coniferous and non-woody species in a literature survey conducted on elevated- $\text{CO}_2$  experiments over the last 40 years (Domec et al., 2016a). As shown in Table 2, the needle size, phloem diameter and the number of phloem cells per needle appear to be suppressed by increased atmospheric  $\text{CO}_2$ . When

accounting for all the loading leaf at the canopy-level, the enhancement of canopy leaf area ( $\sim 16\%$ ) (McCarthy et al., 2007) results in 35.6% decrease in  $K_{\max}$  but a nearly unaltered  $V_p$  (i.e., 5.8% decrease). Hence, the expenditure of water loss,  $\lambda_X$ , is predicted by Eq. (16) to increase by 65.1%, comparable with the percentage increase of  $\lambda_X$  (i.e., 62.9%) computed by inverting  $\lambda_X$  based on SOT from leaf-level gas exchange measurements at the same site (Katul et al., 2010). Furthermore, the difference in photosynthetic parameters of *Pinus taeda* L. between control- and elevated- $\text{CO}_2$  plots is not significant (Ellsworth et al., 2012; Katul et al., 2010). It was assumed here that acclimation of  $k_1$  and  $k_2$  did not occur (e.g., no down-regulation). If  $\lambda_X$  is the only plant trait to be modified by elevated- $\text{CO}_2$ , the general trends in decreasing  $g_{s,ww}$  and  $c_i/c_a$  ratio and increasing  $f_c$  and WUE with increasing  $c_a$  (Ellsworth et al., 2012; Katul et al., 2010) can be attributed to the combined effects of increasing  $\lambda_X$  and  $c_a$  (i.e., Eq. (21)). However, the suppression of  $g_{s,ww}$  and  $c_i/c_a$  ratio by increasing  $\lambda_X$  is relatively small (Ellsworth et al., 2012; Katul et al., 2010) when compared with the sensitivity of  $f_c$  and WUE to long-term elevated- $\text{CO}_2$ . The increment of  $c_a$  in the numerator of  $f_c$  and WUE further amplifies the effects of elevated- $\text{CO}_2$  on  $f_c$  and WUE.

### 3.4. Study limitation

Given all the assumptions made to arrive at the proposed modeling approach, it is instructive to present future improvements to the current formulation while retaining a quasi-steady assumption for analytical tractability. As suggested in a recent review of SOT (Buckley et al., 2016), aerodynamic modifications resulting from the interaction between wind speed and the leaf (represented by boundary-layer conductance;  $g_b$ ) and the  $\text{CO}_2$  transport efficiency in the mesophyll (encoded in the mesophyll conductance;  $g_m$ ) are required when their magnitudes are comparable with  $g_s$ . Regarding  $g_b$ , the stomatal behavior can be altered appreciably by  $g_b$  even when the state variables such as  $T_a$ ,  $\text{CO}_2$  and water vapor concentrations above the laminar boundary layer remain the same (Huang et al., 2015; Schymanski and Or, 2016). The effects of  $g_b$  on  $g_s$  have been incorporated into prior models using SOT or profit-maximization (Huang et al., 2015; Sperry et al., 2016a; Wolf et al., 2016). However,  $g_b$  was mainly characterized by mean wind speed and effective leaf size using empirical formulations that may not reflect wind contact angle, leaf orientation and the micro-roughness on the leaf surface, and turbulent intensity. With regard to  $g_m$ , the effects of  $g_m$  on  $f_c$  has been considered explicitly in some SOT (Volpe et al., 2011) and compared with empirical data to explore the partitioning between  $g_s$  and  $g_m$  under salt-stressed conditions when soil water availability is not limited. Evidence that  $g_m$  is finite and varies with various environmental factors has been reviewed elsewhere (Flexas et al., 2008), with  $g_m$  being reduced during persistent drought conditions (Grassi and Magnani, 2005; Jones, 1973). As suggested elsewhere (Gu and Sun, 2014), however, the dependency of  $g_m$  on  $c_i$  or irradiance may be artifacts due to measurement methods.

Uncertainties in modeling  $g_s$  can be further reduced when the spatio-temporal dynamics of water movement in the soil-xylem hydraulic system are appropriately described. Plant water storage (PWS) and hydraulic redistribution (HR) representing above- and below ground water reservoirs are the two defining features that impact soil-plant hydrodynamics and drought resilience (Domec et al., 2010; Goldstein et al., 1998; Huang et al., 2017; Maherali and DeLucia, 2001; Neumann and Cardon, 2012; Prieto et al., 2012; Stratton et al., 2000). To accommodate the overnight competition for water between PWS and HR in modeling  $g_s$ , a multi-layered scheme for solving water mass balance in each soil-plant compartments is required (Huang et al., 2017). The consideration of how the soil-xylem hydraulics (i.e.,  $K - \psi_i$  relation) is impacted by the delay refilling processes in air-filled xylem conduits (Brodribb and Cochard, 2009; Sperry and Tyree, 1990) is also required especially when the function of impaired xylem conduits cannot be recovered under water stress condition. When coupled with light attenuation and turbulent flow models, detailed representation of hydraulic architec-

ture (Bohrer et al., 2005; Hentschel et al., 2013; Janott et al., 2011; Manoli et al., 2014; 2017) for individual plant can further assist understanding plant-plant competition for water and light. Despite the plethora of complications to measure or model water relations with the soil-plant system, an exhaustive theoretical treatment for the aforementioned mechanisms may also shed light on how the transport of chemical signals (e.g., abscisic acid) through xylem contributes to stomatal behavior (Tardieu, 2016).

In line with recent studies (Hölttä et al., 2017; Jensen et al., 2016; Lucas et al., 2013; Nikinmaa et al., 2013; Sevanto, 2014; Stroock et al., 2014), the significance of the phloem anatomy and physiology associated with long-distance sucrose transport on  $g_s$  cannot be overlooked. At the whole-plant level, sucrose export from the loading phloem here requires further elaboration to account for influences of loading efficiencies with different loading strategies, viscosity built-up due to sucrose accumulation, elastic nature of sieve element, thickness of the sieve plate and distribution of sieve pore radii (Jensen et al., 2012; 2014; Liesche et al., 2015; Thompson and Holbrook, 2003; Turgeon, 2010). How the modifications of osmotic regulation in response to drought stress in each plant compartment impact the transport system (Dichio et al., 2006; Morgan, 1984) should be also accounted for in future modeling efforts. However, the primary challenge remains at the long time-scales. Different from quantifying short time-scales stomatal responses, the difficulty in evaluating how acclimation or adaptation of plant traits respond to the history of environmental conditions can be further accentuated by the fact that the climate system is also sensitive to feedbacks from plants, thereby generating the so-called *feedback cycle*.

## 4. Conclusion

The significance of biotic controls through stomata on global carbon and water cycles, food production and security, and ecosystem services is rarely disputed. We developed a mathematical model of stomata based on the premise of a coordinated photosynthetic-hydraulic-sucrose transporting machinery. We hypothesize that this coordination evolved to maximize the sucrose mass flux out of the loading leaf. Because we consider that maximizing sucrose mass flux can be readily viewed as maximizing energy flux, we proposed this as a qualitative link to Lodka's maximum energy circulation principle in plants. For a wide range of time-scales, the proposed approach captures the general features of stomatal sensitivity to environmental factors and hydrological states. The proposed framework explains how the carbon and water economies are intrinsically linked by the coordination among the main mass transporting networks within plants that dictates the much debated isohydric-to-anisohydric behavior. To permit analytical foresight, only the main transporting processes impacting  $g_s$  are accounted for in the soil-xylem-leaf-phloem system. Variable sucrose sinks and stores from the loading to the unloading zones were not explicitly treated here. Recent research trends are beginning to address carbon allocation and sinks throughout the entire plant system (Fatichi et al., 2014; Hartmann and Trumbore, 2016; Savage et al., 2015) and the framework here must be viewed as one step in this direction. It offers immanent constraints as to how  $g_s$  responds to its environment on multiple time-scales pertinent to the xylem-leaf-phloem transport system. Field and laboratory testing of the proposed approach here are topics for future studies.

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## Appendix A. Model derivation

When combining Eqs. (7)–(10),  $F_E$  can be expressed as:

$$F_E = Q_c \frac{N_c}{V_p} A_{xp} L_{xp} \left( \psi_l + RT_p \frac{N_c}{V_p} - p_g \right). \quad (\text{A.1})$$

In Eq. (A.1), mechanical pressure ( $p_p$ ) is assumed to be negligible when compared with osmotic potential ( $\Pi = -RT_p N_c/V_p$ ) over a short period (Jensen et al., 2016). By substituting Eq. (6) into Eq. (A.1),  $F_E$  can be now written as a function of  $\psi_l$ :

$$F_E(\psi_l) = G [f_c^2(\psi_l) + I(\psi_l - p_g) f_c(\psi_l)], \quad (\text{A.2})$$

where  $G = Q_c A_{xp} L_{xp} RT_p (\alpha \beta A_l \Delta t / V_p)^2$  and  $I = (V_p / A_l) (\alpha \beta \Delta t RT_p)^{-1}$ . When coupling the supply-demand balance of  $\text{CO}_2$  (i.e.,  $f_{c,s} = f_{c,d}$ ; Eq. (2)) and water (i.e.,  $f_{e,s} = f_{e,d}$ ; Eq. (4)) fluxes through  $g_s$ ,  $f_c$  in Eq. (A.2) can be written as a function of  $\psi_l$  and directly reflects the limitations imposed by the photosynthetic machinery and soil-xylem hydraulics on  $F_E$  (see Section 1).

Now, inserting Eq. (4) (i.e.,  $\psi_l = \psi_s - (m_v A_l f_e(\psi_l)) / K(\psi_l)$ ) into Eq. (A.2) to replace  $\psi_l$ , Eq. (A.2) can be re-written as:

$$F_E(\psi_l) = G \left[ f_c^2(\psi_l) + I \left( \psi_s - \frac{m_v A_l f_e(\psi_l)}{K(\psi_l)} - p_g \right) f_c(\psi_l) \right]. \quad (\text{A.3})$$

Under well-watered soil condition (i.e.,  $\psi_s \approx 0$ ) with negligible  $p_g$ , the export of energy flux from loading phloem ( $F_{E,ww}(\psi_l)$ ) is subsequently approximated as:

$$F_{E,ww}(\psi_l) = G \left[ f_c^2(\psi_l) + m_v I A_l \frac{f_e(\psi_l)}{K(\psi_l)} f_c(\psi_l) \right]. \quad (\text{A.4})$$

Thus, the optimal  $\psi_{opt}$  can be obtained by setting  $\partial F_{E,ww} / \partial \psi_l = 0$  that yields:

$$\frac{\partial f_c(\psi_l)}{\partial \psi_l} - \frac{m_v I A_l}{2} \left[ \underbrace{\frac{f_e(\psi_l)}{K(\psi_l) f_c(\psi_l)} \frac{\partial f_c(\psi_l)}{\partial \psi_l}}_M + \underbrace{\frac{\partial}{\partial \psi_l} \left( \frac{f_e(\psi_l)}{K(\psi_l)} \right)}_N \right] = 0. \quad (\text{A.5})$$

When  $M/N \ll 1$  (see Appendix B), Eq. (A.5) is reduced to:

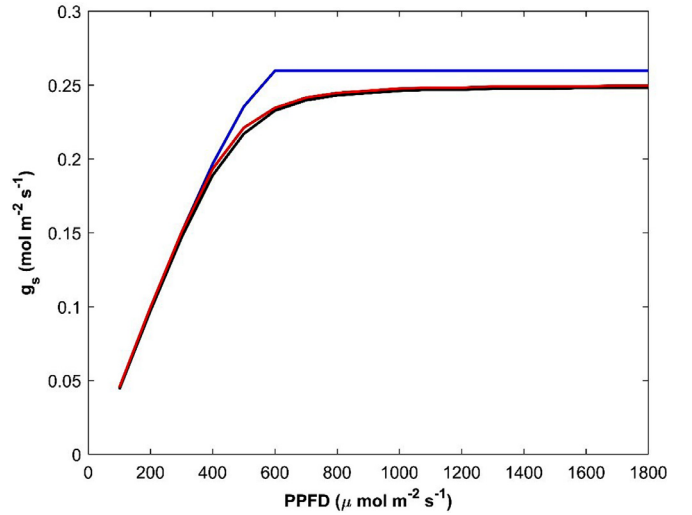
$$\frac{\partial f_c(\psi_l)}{\partial \psi_l} - \frac{m_v I A_l}{2} \frac{\partial}{\partial \psi_l} \left( \frac{f_e(\psi_l)}{K(\psi_l)} \right) = 0. \quad (\text{A.6})$$

or

$$\frac{\partial}{\partial \psi_l} \left[ f_c(\psi_l) + \frac{I}{2} \psi_l \right] = 0, \quad (\text{A.7})$$

At  $\psi_s \approx 0$ , the reduction in  $K(\psi_l)$  is small and  $K(\psi_l)$  can be approximated as  $K_{max}$  (see Appendix B) so that Eq. (A.6) can be further simplified as:

$$\frac{\partial}{\partial \psi_l} \left[ f_c(\psi_l) - \frac{m_v I A_l}{2 K_{max}} f_e(\psi_l) \right] = 0. \quad (\text{A.8})$$



**Fig. Appendix B.1.** Modeled stomatal conductance ( $g_s$ ) as a function of photosynthetically active radiation (PPFD) under well-watered condition. The model results calculated from Eqs. (A.2), (A.7) and (A.8) are respectively represented by black, red and blue lines. The physiological, hydraulic and allometric attributes of soil-plant system for coniferous species in general reported elsewhere (Huang et al., 2017) are adopted. Physical characteristics of leaves and anatomical attributes of phloem for *Pinus taeda* L. listed in Table 2 are used.  $T_a$ ,  $c_a$  and  $RH$  are respectively fixed to be 25 °C, 400 ppm and 50% while PPFD varies from 100 to 1000  $\text{mol m}^{-2} \text{s}^{-1}$ . (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

## Appendix B. Scaling analysis

In Eq. (14), the ratio of M to N can be approximated as:

$$\frac{M}{N} = \frac{f_e \frac{\partial f_c}{\partial \psi_l}}{K f_c \frac{\partial}{\partial \psi_l} \left( \frac{f_e}{K} \right)} \approx \frac{f_c^{-1}}{f_e} \frac{\partial f_c}{\partial f_e} \left( 1 + \frac{\partial K}{K} \frac{\partial \psi_l}{\partial \psi_l} \right), \quad (\text{B.1})$$

where  $f_c/f_e$  is the water use efficiency on the order of  $10^{-3}$  (Huang et al., 2015; Schymanski and Or, 2016),  $\partial f_c / \partial f_e$  is the marginal water use efficiency on the order of  $10^{-4}$ – $10^{-3}$  (Lloyd and Farquhar, 1994; Manzoni et al., 2011),  $\partial K / K \approx -10^{-1}$  is the percentage of  $K$  loss referenced to maximum  $K_{max}$  at  $\psi_s \approx 0$  (i.e., operating  $K \approx K_{max}$ ) and  $\psi_l / \partial \psi_l$  is on the order of 1 because stomatal closure commonly occurs before the air-entry point (i.e., at  $\psi_l$  where 12% of  $K$  losses occur) (Bond and Kavanagh, 1999; Sparks and Black, 1999), so that  $M/N \ll 1$ .

As shown in Fig. B.1, the difference of modeled  $g_s$  between Eqs. (A.8) and (A.2) (or (A.7)) increases with increasing  $f_e$  (i.e., a larger PPFD) when soil water status is close to saturation. However, such small difference (i.e., less than 10%) suggests that the approximation of  $M/N \ll 1$  and the assumption of  $K \approx K_{max}$  adopted in Eq. (A.8) do not significantly impact the model results. If the plant allows that the percentage of  $K$  losses can be much larger than 12% (i.e., operating  $K \ll K_{max}$ ), M in Eq. (A.5) cannot be ignored and Eq. (A.2) is required.

## Appendix C. Analytical solution and its approximation of stomatal optimization theory (SOT) under well-watered soil condition

When the supply-demand balance of  $\text{CO}_2$  and water fluxes is incorporated into SOT,  $g_s$ ,  $c_i$  and  $\psi_l$  can be interchangeable independent variables. For convenience,  $c_i$  is selected here as the independent variable and the inverse of  $\lambda_X(\Lambda)$  is adopted (Medlyn et al., 2011; Prentice et al., 2014) to derive the analytical solution from SOT, in which the Hamiltonian can be now given as:

$$H_{a,X}(c_i) = f_e(c_i) - \Lambda f_c(c_i). \quad (\text{C.1})$$

Assuming  $R_d$  is negligible when compared with  $f_c$ , the optimal  $c_i$  can be obtained by setting  $\partial H_{a,x}(c_i)/\partial c_i = 0$  and is equivalent to the positive root of quadratic function,  $Ac_i^2 + Bc_i + C = 0$ , where:

$$\begin{aligned} A &= L - (k_2 + \Gamma^*), \\ B &= 2(k_2 + \Gamma^*)c_a - 2L\Gamma^*, \\ C &= -(k_2 + \Gamma^*)c_a^2 + (k_2 + \Gamma^*)Lc_a - k_2\Gamma^*L, \end{aligned} \quad (C.2)$$

where  $L = aD/\Lambda$ . If  $c_i \gg \Gamma^*$  is further assumed, the determinant of quadratic function can be subsequently simplified to (Medlyn et al., 2011):

$$\Delta \approx 4L(k_2 + \Gamma^*)c_a^2. \quad (C.3)$$

Thus, the optimal  $c_i$  can be given as:

$$c_i = \frac{-(k_2 + \Gamma^*)c_a + L\Gamma^* + c_a\sqrt{L(k_2 + \Gamma^*)}}{L - (k_2 + \Gamma^*)}. \quad (C.4)$$

Because  $c_a > c_i \gg \Gamma^*$ ,  $c_i/c_a$  ratio can be approximated as:

$$\frac{c_i}{c_a} \approx \frac{(k_2 + \Gamma^*) - \sqrt{L(k_2 + \Gamma^*)}}{(k_2 + \Gamma^*) - L}. \quad (C.5)$$

By substituting  $L = aD/\Lambda$  and  $\Lambda = 1/\lambda_X$  into Eq. (C.5),  $c_i/c_a$  ratio and the corresponding  $g_{s,ww}$  can be now written as:

$$\begin{aligned} \frac{c_i}{c_a} &= \frac{1}{1 + \sqrt{\frac{aD\lambda_X}{k_2 + \Gamma^*}}} = \frac{\sqrt{\frac{k_2 + \Gamma^*}{a\lambda_X}}}{\sqrt{\frac{k_2 + \Gamma^*}{a\lambda_X}} + \sqrt{D}}, \\ g_{s,ww} &= \left(1 + \sqrt{\frac{k_2 + \Gamma^*}{aD\lambda_X}}\right) \frac{f_c}{c_a}. \end{aligned} \quad (C.6)$$

The  $c_i/c_a$  ratio in Eq. (C.6) can be also expressed by Taylor series expansion that is given as:

$$\frac{c_i}{c_a} = \frac{1}{1 + \chi} \approx \sum_n (-\chi)^n. \quad (C.7)$$

where  $\chi = \sqrt{aD\lambda_X/(k_2 + \Gamma^*)}$  and  $n \in (0, \infty)$  is zero or a positive integer. When  $\chi$  is relatively small, the higher order terms in Eq. (C.7) can be neglected, leading to the approximation of  $c_i/c_a$  ratio and  $g_{s,ww}$  that is given as:

$$\begin{aligned} \frac{c_i}{c_a} &= 1 - \sqrt{\frac{a\lambda_X}{k_2 + \Gamma^*}} \sqrt{D}, \\ g_{s,ww} &= \sqrt{\frac{k_2 + \Gamma^*}{a\lambda_X}} \frac{f_c}{c_a} D^{-1/2}. \end{aligned} \quad (C.8)$$

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